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Transformer Oil Ageing Detection using Mach-Zender Interferometry Configuration as a Sensor

D.Vinoth¹, P.Iranbu², Prasanth A³, Ajithkumar V⁴, Ashokkumar K⁵

Assistant Professor, Department of Electrical and Electronics Engineering, Muthayammal College of Engineering,
Namakkal, Tamil Nadu, India.^{1,2},

UG Scholar, Department of Electrical and Electronics Engineering, Muthayammal College of Engineering, Namakkal,
Tamil Nadu, India^{3,4,5}

ABSTRACT: System for monitoring oil level and detecting leaks in power transformers, reactors, current and potential transformers, high voltage bushings and the like, notably for a system that through the use of sensors and other electronic components measures and monitors transformers and similar equipment in real time, filled with insulating oil, with greater precision and without need for floats or mobile mechanical parts, while presenting countless facilities in the sense of making level monitoring more reliable and safer, highlighting the level error calculations, oil leak detection alarm, excess oil detection alarm during the equipment filling process and calculation of tendencies of evolution for levels among other facilities.

KEYWORDS : Transformer oil, Ageing measurement, Mach-Zender interferometry, Bare fibre, Chemical etching

I. INTRODUCTION

Power transformers and reactors are pieces of equipment widely used in medium, high and extra-high voltage electric power generation, transmission and distribution systems. These devices frequently use for insulation and heat removal some type of oil, which can be mineral (petroleum by product), vegetal (from soy bean, sunflower or other) or silicon, for example. [0003] Transformers and reactors have copper coils that are wrapped in paper. The entire active part - comprised of a core and coils - is then immersed in insulating oil to impregnate the paper and thus ensure the electric isolation of the assembly, and to cool the coils with the oil circulating in heat radiation is removed; these properties increase the sensitivity of optical sensors to the surrounding media by C.Nagarajan et al [7,8,9]. In this paper, tapered fibres are used as a sensing arm in the MZI configuration to detect the ageing of transformer oils on the basis of the changing RI. This type of fibre is tapered using hydrofluoric acid (HF, 30%) in accordance with the chemical etching method. The results are compared with those of a standard AC breakdown voltage test and oil absorption test for validation.

II. PRINCIPLES OF TAPERED OPTICAL FIBRESENSOR

Light signals are propagated in the optical fibre wave guide in accordance with the theory of total internal reflection. The reflections are due to the differences between the RI of the core and the cladding of the optical fibre. When the cladding is tapered by reducing its diameter, light penetrates the fibre wall as an evanescent field. The evanescent field is affected by the surrounding medium. The surrounding medium is transformer oil, which functions as a new cladding. Tapering the fibre changes two parameters, namely, the number of light reflections and the incident angle. The reflection

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is increased when the incident angle reaches the critical angle (ϕ_c). The sensitivity of the optical fibre is affected by the changes in the tapered ratio (TR), as in reference [22].

$$TR = \frac{P}{P_0} \quad (1)$$

Where TR is the tapered ratio, P is the waist in μm and P_0 is the core radius in μm . Factors such as core RI, cladding RI and external RI affect the light propagated inside fibres. The evanescent field extends from the core cladding interface to the penetration depth dp , as shown in Fig. 2. The value of dp is derived using Equation (2).

$$dp = \frac{\lambda}{2\pi\sqrt{n_{cl}^2 \sin^2 \theta - n_{ex}^2}} \quad (2)$$

θ is the incident angle, λ is the wavelength, n_{cl} is the cladding refractive index and n_{ex} is the external refractive index (RI of the transformer oil).

As shown in Fig. 2, the value of dp is small and cannot reach the surrounding medium. Thus, the tapering technique is used to allow evanescent fields to penetrate the surrounding medium. In this study, the surrounding medium is transformer oil, and the fibre is tapered using HF as an etchant solution in accordance with the chemical etching method.

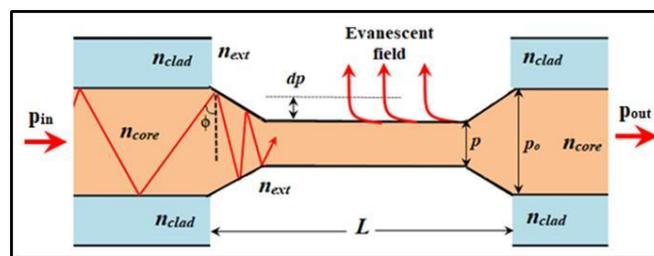


Fig. 1. Cross section of the sensing arm

III. EXPERIMENTAL PROCEDURE AND MEASUREMENT

A. Sensor fabrication

The fabrication of a bare optical fibre sensor is implemented by chemical etching using 30% HF. A Plexiglass piece (100 mm \times 50 mm \times 10 mm) is used as an etching reactor. The depth of the etching chamber is 5 mm. The Plexiglas material is lightweight and corrosion resistant. The setup for etching process is shown in Fig. 3.

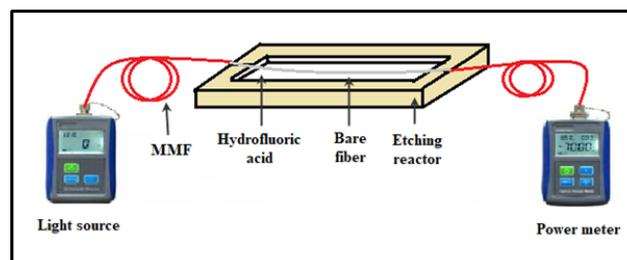


Fig. 2. Schematic diagram of setup for etching process.

The type of fibre used in this experiment is multimode fibre MMF 50/125 μm core/cladding diameter multimode fibre, and the bare length is 8 cm. The cladding is removed from the optical fibre under 60 min of etching. Throughout the

etching process, the sending end of the optical fibre is connected to a (10 mW, 650 nm) laser light source, whereas the receiving end is connected to a power meter (NESTONG T1102). The etching is monitored and controlled on the basis of the light power (nW) measured at the receiving end. The etching is stopped when the output power is approximately 35% of the total initial power before etching; the removal of the MMF cladding lasts approximately 60 minutes. The characteristics of the output power during etching are shown in Fig. 4. In this figure, the no evanescent field region is starting from (0-24) minute. At this time of etching process, the cladding is not affected by HF, so no evanescent field propagate to fibre wall. The weak evanescent region is started from (24-40) minute. The light starts to propagate to the fibre wall because the fibre cladding is reduced by the effect of HF. At the strong evanescent field (40-60) minute, the HF reached to the core of fibre that is made by glass, so more of lights is propagated to the fibre wall because the core (glass) is highly affected by the HF than cladding.

At the last stage of etching process, a distilled water is used to wash the fibre from the HF. At this point, the etching process is stopped, and the output power is stable.

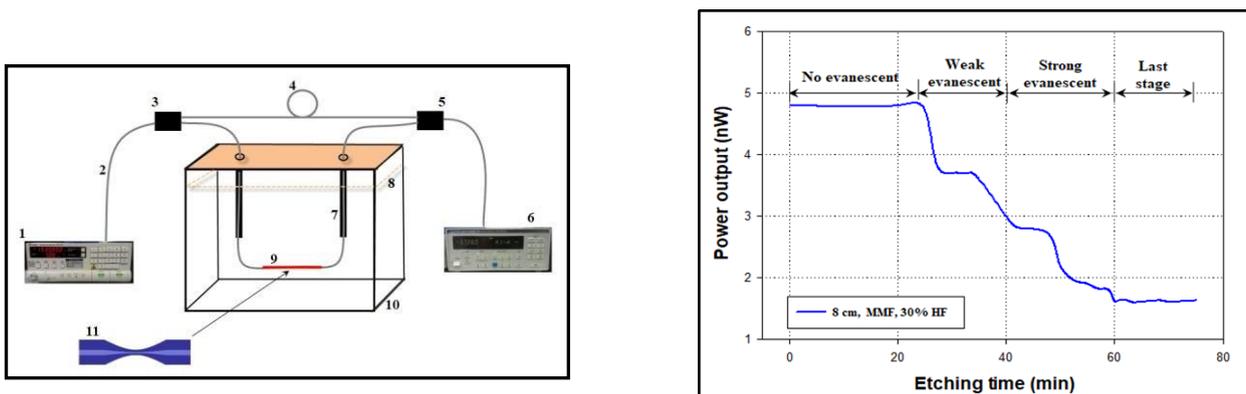


Fig. 4. Optical output power vs. etching time using 30% HF solution.

B. Experimental setup and preparation of transformer oil sample

The bare optical fibre functions as the sensing arm of the MZI configuration. The schematic of the experimental setup using the MZI configuration is shown in Fig. 5 and Table 1 shows the details for each label in the figure. As shown in this figure, the first optical coupler splits the light into two parts (i.e., sensing arm and reference arm). The sensing arm is immersed in transformer oil, whilst the reference arm is not. The second optical coupler then collects the light and sends it to the power meter at the receiving end of the MZI configuration.

In this study, five samples of mineral oil (Libra) are used. S1 is fresh oil used as a reference, and S2, S3, S4 and S5 are different samples of aged oil prepared by thermal accelerated ageing. In the accelerated ageing process, four types of metal substances (Cu, Fe, Zn and Al) are added into fresh oil according to reference [23]. The resulting mixture is then placed in an oven at 120 °C for different ageing times. The heat inside the oven increases the ageing rate, as shown in Equations (3), (4) and (5) [24] [25]. If the temperature increases to 7 °C, then the rate of degradation is doubled. The normal operating temperature of transformer oil is 60 °C. Hence, one day of laboratory ageing (inside an oven) is equivalent to a year in the field [1]. Table 2 shows the description of the samples for different ageing times and metal substances.

$$t_f = t_k \times 2^{\left(\frac{T_k - 60}{7}\right)} \quad (3)$$

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Where t_f is the equivalent time of ageing, t_k is the aging

period and T_K is the accelerated aging temperature.

$$\text{Aging accelerating factor} = \frac{120^\circ\text{C} - 60^\circ\text{C}}{7^\circ\text{C}} = 8.57$$

$$\text{Time factor} = 2^{8.57} = 380 \text{ days}$$

Fig. 5. Schematic of the experimental setup.

Table- I: Details of the test setup

Label	Description
1	Light source, Santec WSL-100, 1550 nm
2	MMF, Core/cladding diameter: 50.0/125 μm RI, Core/cladding: 1.500/1.485
3, 5	Coupler (1, 2): 50/50 %
4	Reference arm, MMF
6	Optical power meter, ILX Light wave (OMM-6810B)
7	Holder
8	Transformer oil level
9	Sensing arm
10	Tank
11	Tapered fiber

Table- II: Description of samples

Sample name	Time of aging	Equivalent durations in fields (Days/Years)	Metal substance
Sample S1	0 hour	0/0	0 g/l
Sample S2	48 hours	2/2	Cu= 2.5 g/l
Sample S3	96 hours	4/4	Fe= 2.5 g/l
Sample S4	144 hours	6/6	Zn= 0.5 g/l
Sample S5	192 hours	8/8	Al= 0.5 g/l

C. Results and discussion

Measuring RI depends on the speed of light inside transformer oils. Oil contamination decreases the speed of light propagating inside transformer oils. Figure 6 illustrates the RI of the transformer oil samples measured at 24 °C using a digital refractometer (DR102). The RI of this device ranges from 1.3330 to 1.5177. As shown in Fig. 6, the RI of fresh oil is 1.4611, while that of aged oil is 1.4722. Hence, as the time of ageing increases, the RI increases.

A breakdown voltage test is conducted on the five samples according to the standard ASTM D1816-84a [26]. The high ageing transformer oil has low breakdown voltage and high RI; the opposite is true for the low ageing samples.

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The moisture and chemical decomposition of the conducting material increase due to the temperature and ageing process. As such, the internal characteristics of the transformer oil changes, thereby reducing the quality of the oil and the value of the breakdown voltage. Fig. 7 illustrates the characteristics of the RI and breakdown versus time of ageing.

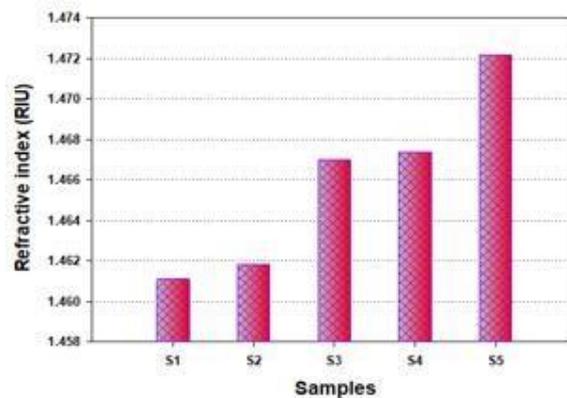


Fig. 6. Refractive index of oil samples at 24 °C.

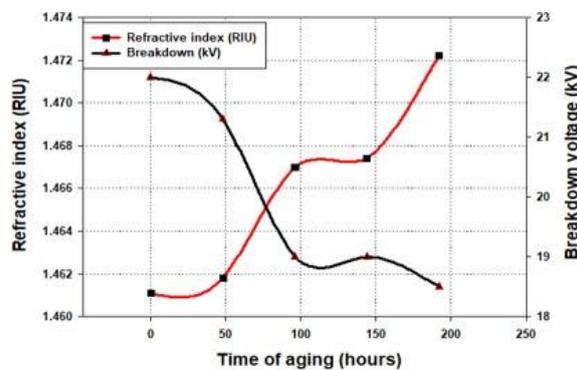


Figure 7: Refractive index and breakdown vs. time of ageing

A laser Santec WSL-100 light source projects light to the sending end of the MZI configuration. The light is divided into two parts by the first optical coupler 50/50%. This coupler sends the light to the sensing and reference arms. The sensing arm is a tapered MMF fibre immersed in transformer oil, as shown in Figure 5. The second coupler functions as a summation device that collects the light from the reference and sensing arms and then sends the light to the receiving end of the MZI configuration. At the receiving end, the power intensity of the light is measured by using an ILX light wave power meter. Fig. 8 illustrates the characteristics of the output power of the MZI sensor and the value of the breakdown voltage for all samples.

The RI of the transformer oil changes because of different thermal ageing times. A low-quality transformer oil has a high RI, whereas a high-quality transformer oil has a low RI. At the sensing arm of the MZI configuration, the light leaks out to the surrounding medium (i.e., transformer oil) as the evanescent field. The quantity of the light that leaks out depends on the RI of the transformer oil. Thus, we obtain at the receiving end a high output power for a low-quality transformer oil and a low output power for fresh oil.

The absorption spectrum signal of the transformer oil is measured from 355 nm to 405 nm by using a UV-visible spectrophotometer (SHIMADZU, UV-1800), as shown in

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Fig. 9. In this figure, the low-quality transformer oil has a higher absorption spectrum than the high-quality oil does. The characteristics of the absorption spectrum differ for various oil samples because the physical properties of transformer oils are different and depend on the thermal ageing time.

From above, it seems the correlation is clear between the oil breakdown test, refractive index and absorption spectrum test. When the oil is degrade, the value of breakdown voltage will decrease and at the same time the RI increases. On the other hand, the oil absorption spectrum will be increased. So, the MZI sensor can detect the ageing of transformer oil based on different output power.

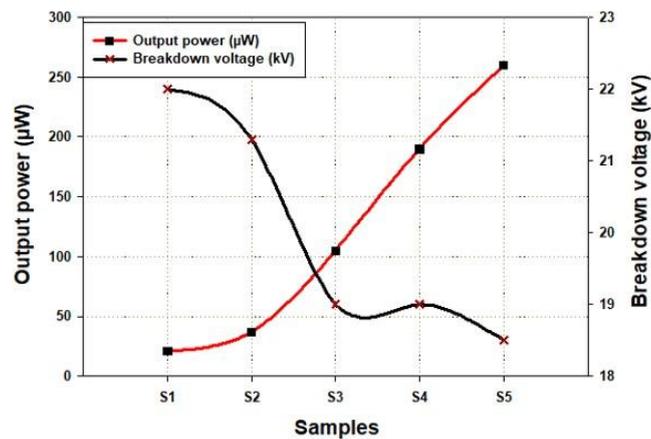


Fig. 8. Characteristics of output power and breakdown voltage.

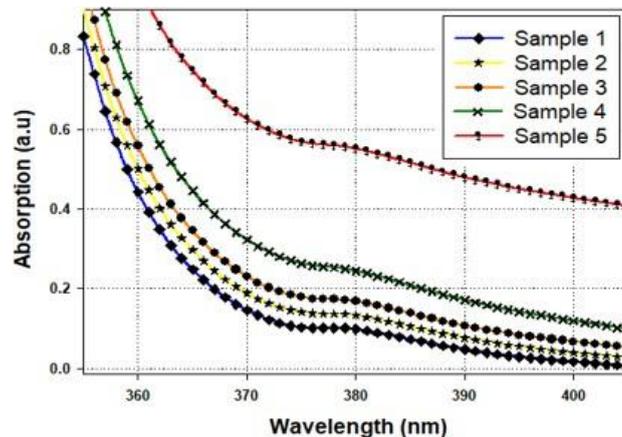


Fig. 9 Absorption spectrum signal of transformer oil samples

IV. CONCLUSION

A fibre optic sensor based on MZI configuration was developed with a bare fibre as the sensing arm of the sensor. The fibre cladding was removed by chemical etching using HF as an etchant. The sensor was affected by the RI of the transformer oils. Moreover, it could detect the ageing of transformer oils on the basis of the changes in its RI. As a result, the output power of the MZI sensor was affected by the quality of the transformer oil (i.e., transformer oil RI).

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The results showed that the output power is in line with the breakdown voltage test. The sensor output has correlation with the oil absorption spectrum test. This study is important in improving the online monitoring of high voltage transformers as it provides early information about the quality of transformer oils and thus increases the reliability of power system networks.

REFERENCES

- [1] G M. Kohtoh, G. Ueta, S. Okabe, and T. Amimoto, "Transformer insulating oil characteristic changes observed using accelerated degradation in consideration of field transformer conditions," *IEEE Transactions on Dielectrics and Electrical Insulation*, vol. 17, no. 3, pp. 808–818, 2010.
- [2] M. A. Salam, Q. M. Rahman, F. Wen, S. P. Ang, and W. Voon, "Causes of transformer failures and diagnostic methods – A review," *Renewable and Sustainable Energy Reviews*, vol. 82, pp. 1442–1456, 2018.
- [3] M. Wang, A. J. Vandermaar, and K. D. Srivastava, "Review of condition assessment of power transformers in service," *IEEE Electrical insulation magazine*, vol. 18, no. 6, pp. 12–25, 2002.
- [4] M. Bagheri, M. S. Naderi, T. Blackburn, and B. T. Phung, "Dean-Stark vs FDS and KFT methods in moisture content recognition of transformers," In *Power and Energy (PECon), 2012 IEEE International Conference*, no. December, pp. 712–717, 2012.
- [5] I. Hurezeanu, C. I. Nicola, D. Sacerdotianu, M. Nicola, A. M. Aciu, and
- [6] M. C. Nitu, "Temperature control and monitoring system for power transformer windings using fiber optic sensors," *Fundamentals of Electrical Engineering (ISFEE), 2016 International Symposium on*. IEEE, 2016., pp. 1–4, 2016.
- [7] C.Nagarajan and M.Madheswaran - 'Stability Analysis of Series Parallel Resonant Converter with Fuzzy Logic Controller Using State Space Techniques' - *Electric Power Components and Systems*, Vol.39 (8), pp.780-793, May 2011
- [8] E Geetha, C Nagarajan, "Induction Motor Fault Detection and Classification Using Current Signature Analysis Technique", 2018 Conference on Emerging Devices and Smart Systems (ICEDSS), 2nd and 3rd March 2018, organized by mahendra Engineering College, Mallasamudram, PP. 48-52,2018
- [9] Nagarajan, M.Madheswaran and D.Ramasubramanian- 'Development of DSP based Robust Control Method for General Resonant Converter Topologies using Transfer Function Model' - *Acta Electrotechnica et Informatica Journal* , Vol.13 (2), pp.18-31, April-June.2013