

Performance Assessment of Heat Exchanger Using Mamdani Based Adaptive Neuro-Fuzzy Inference System (M-ANFIS) and Dynamic Fuzzy Reliability Modeling

¹Pravin Kumar Borkar, ²Manoj Jha, ³M. F. Qureshi, ⁴G.K.Agrawal

¹Department of Mechanical Engg., Rungta College of Engg. & Tech., Raipur, India.

²Department of Applied Mathematics, RSR Rungta College of Engg. & Tech., Raipur, India.

³Department of Electrical Engg., Govt. Polytechnic, Janjgir-Chapa, India.

⁴Department of Mechanical Engg., Govt. Engg. College, Bilaspur, India.

ABSTRACT: Performance monitoring system for shell and tube heat exchanger is developed using Mamdani Adaptive Neuro-Fuzzy Inference System (M-ANFIS). Experiments are conducted based on full factorial design of experiments to develop a model using the parameters such as temperatures and flow rates. M-ANFIS model for overall heat transfer coefficient of a design /clean heat exchanger system is developed. The developed model is validated and tested by comparing the results with the experimental results. This model is used to assess the performance of heat exchanger with the real/fouled system. The performance degradation is expressed using fouling factor (FF), which is derived from the overall heat transfer coefficient of design system and real system. Hybrid algorithm is the hot issue in Computational Intelligence (CI) study. From in-depth discussion on Simulation Mechanism Based (SMB) classification method and composite patterns, this paper presents the Mamdani model based Adaptive Neural Fuzzy Inference System (M-ANFIS) and weight updating formula in consideration with qualitative representation of inference consequent parts in fuzzy neural networks. M-ANFIS model adopts Mamdani fuzzy inference system which has advantages in consequent part. Experiment results of applying M-ANFIS to evaluate Reliable Performance Assessment of Heat Exchanger show that M-ANFIS, as a new hybrid algorithm in computational intelligence, has great advantages in non-linear modeling, membership functions in consequent parts, scale of training data and amount of adjusted parameters. This paper proposes a new perspective and methodology to model the fouling factor (FF) of the heat exchanger using the fuzzy reliability theory. We propose to use the indicator or performance or substitute variable which is very well understood by the power plant engineer to fuzzify the states of heat exchanger.

KEYWORDS: Heat exchanger; Overall heat transfer coefficient; Fouling factor (FF), Fuzzy reliability, performance characteristics, Mamdani Adaptive Neuro-Fuzzy Inference System (M-ANFIS).

I.INTRODUCTION

Heat exchanger process is complex due to its nonlinear dynamics and particularly the variable steady state gain and time constant with the process fluid (Mandanvane et al 2006). Heat exchangers are used to transfer the heat between two fluids across a solid surface that are at different temperatures. The commonly used shell and tube heat exchangers are used in refrigeration, power generation, heating, air conditioning, chemical processes, manufacturing and medical applications (Ozcelik, 2007). The performance of heat exchanger deteriorates with time due to formation of fouling on heat transfer surface. It is a very complicated phenomenon and can be broadly categorized into particulate, corrosion, biological, crystallization, chemical reaction and freeze. It is necessary to assess periodically the heat exchanger performance, in order to maintain at high efficiency level. Performance of heat exchanger is monitored by the following methods: i) Outlet temperature of the hot stream (T_{ho}) profile, ii) Approach temperature ($T_{ho} - T_{ci}$) profile, iii) Log Mean Temperature Difference (LMTD) with time, iv) Heat load profile, and v) Time series of overall heat transfer

International Journal of Innovative Research in Science, Engineering and Technology

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Vol. 3, Issue 9, September 2014

coefficient. The first four methods are widely used and are ineffective in terms of isolating the net impact of fouling from process upsets. But the overall heat transfer coefficient method requires detailed calculations and knowledge of the geometry of the exchangers (Radhakrishnan et al 2007) Any deviation from the heat transfer coefficient of design/clean heat exchanger will indicate the occurrence of fouling(Vijaysa et al 2006). Tubular Exchanger Manufacturing Association recommends an allowable fouling factor (FF) or fouling resistance to tolerate some degree of fouling before cleaning must be undertaken. Hence, monitoring system is needed to assess the performance of heat exchanger. In experimental studies and engineering applications of thermal science, researchers and engineers are expected to reduce experimental data into one or more simple and compact dimensionless heat transfer correlations (Wang et al 2006). The limitations of correlation methods are addressed by computational intelligent (CI) techniques, such as M-ANFIS and fuzzy reliability. M-ANFIS is one of the most powerful computer modeling techniques, based on fuzzy approach, currently being used in many fields of engineering for modeling complex relationships which are difficult to describe with physical models.

In this paper, a performance monitoring system is developed for a shell-and-tube heat exchanger using secondary measurements namely the temperatures and flow rates of the hot and cold fluid (water). Experimental system is developed to investigate the performance of heat exchanger. M-ANFIS is applied to model the heat exchanger with experimental data. The input parameters to develop a model for design/clean heat exchanger are inlet temperature and flow rate of shell and tube side fluids and output is overall heat transfer coefficient (U_{Design}). The overall heat transfer coefficient of real/fouled system (U_{Real}) is calculated using measured values such as inlet temperature, outlet temperature and flow rate of shell and tube side fluids. The heat exchanger performance is assessed by comparing the results of clean/design and fouled/real system. Any deviation from the result of design/clean system indicates that the performance is degraded due to fouling. Its degree of membership is derived from fouling factor (FF) using U_{Design} and U_{Real} . A Mamdani model based Adaptive Neural Fuzzy Inference System, which named M-ANFIS is proposed here. Experimental results show that this model can achieve the desired targets and have a preferable capacity in performance assessment of heat exchanger.

This paper proposes to use the theory and methods for fuzzy sets to model the reliability for a system with continuous stochastic performance degradation. We use the performance characteristic variable which indicates the continuous performance levels of degradable systems to fuzzify the states of a component or system. The engineering or technological performance variable is well understood by the system designers and can be used to represent different degrees of success. Thus, the imprecision in the meaning of success/failure is quantified through the fuzzy success/failure membership function which is defined over the performance characteristic variable. The proposed fuzzy reliability measures provide an alternative to model the continuous state behavior for a system. The dynamic behavior of fuzzy reliability is investigated using the concept of fuzzy random variable under appropriate stochastic performance degradation processes.

II. MAMDANI BASED ADAPTIVE NEURO FUZZY INFERENCE SYSTEM (M-ANFIS)

This paper presents a class of adaptive neural network equivalent of Mamdani fuzzy inference system in its function, which named M-ANFIS. It means adaptive network based fuzzy inference system. Neural network has the great function of dealing with imprecise data by training, while fuzzy logic can deal with the uncertainty of human cognition. The nature of these two methods is a universal approximator and they have the function of non-linear modeling. In fact, neural networks and fuzzy logic have fused very well. Fuzzy neural networks implement main steps of fuzzy inference in an ordered layers of a neural network with an architecture such that the weights to be adjusted in the network, which makes fuzzy inference more closer to actual situation by learning capability of NN. FNN are widely used in a lot of areas. Jang has brought forward Sugeno fuzzy inference model-based ANFIS. This paper will introduce a Mamdani model based Adaptive Neural Fuzzy Inference System (M-ANFIS), which has greater superiority to ANFIS in expression of consequent part and intuitive of fuzzy reasoning. This model will reflect nature of CI much more. The details will be introduced in the following section.

Model Description

The T-S fuzzy inference system works well with linear techniques and guarantees continuity of the output surface (Tan et al 2009). But the T-S fuzzy inference system has difficulties in dealing with the multi-parameter synthetic evaluation; it has difficulties in assigning weight to each input and fuzzy rules. Mamdani model can show its legibility and understandability to the lay people. The Mamdani fuzzy inference system shows its advantage in output expression and is used in this project. We derive the following theorem. Advantages of applying such composite inference methods are that such Mamdani ANFIS model has the ability of learning because of differentiability during computation. The sum-product composition provides the following theorem (Yang et al 2000), see in Eq.1 and Eq.2. Final crisp output when using centroid defuzzification is equal to weighted average of centroids of consequent MFs, where:

$$\psi(r_i) = \omega(r_i) \times a \tag{1}$$

where, $\psi(r_i)$ is the weighted factor of r_i ; r_i is the i^{th} fuzzy rule; $\omega(r_i)$ is the firing strength of r_i ; a is the area of the consequent MFs of r_i .

$$Z_{COA} = \frac{\int_Z \mu_{C_i}(z)zdz}{\int_Z \mu_{C_i}(z)dz} = \frac{\omega_1 a_1 z_1 + \omega_2 a_2 z_2}{\omega_1 a_1 + \omega_2 a_2} = \frac{\omega_1 a_1 \cdot z_1}{\omega_1 a_1} + \frac{\omega_2 a_2 \cdot z_2}{\omega_2 a_2} \tag{2}$$

Where, a_i and z_i are the area and the center of the consequent MF $\mu_{C_i}(z)$ respectively. According to Eq.1 and Eq.2, we obtain corresponding Mamdani ANFIS model after some modifications.

The overall output f is given. $\{b, c, d\}$ are premise parameters and a, z are consequent parameters which need to adjust. The type of membership functions (MFs) of the inputs are generalized bell functions, each MF has 3 nonlinear parameters; each consequent MF has 2 nonlinear parameters which are area and center of the consequent part. Totally, there are 16 parameters in this example. A general M-ANFIS model can be expressed as Fig.1.

Rule 1: If x is A_1 and y is B_1 , then $Z = C_1$;

Rule 2: If x is A_2 and y is B_2 , then $Z = C_2$.

Fuzzification Inference Implication Aggregation Defuzzification

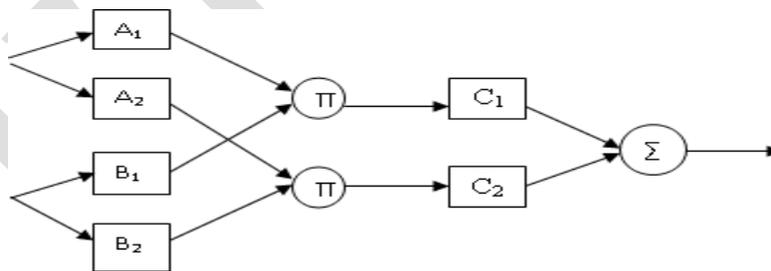


Fig.1 General Model of Mamdani ANFIS

General Mamdani ANFIS architecture consists of five layers, output of each layer is the following.

Layer 1: Fuzzification layer.

$$O_{1,i} = \mu_{A_i}(x), i = 1,2; \tag{3}$$

$$O_{1,i} = \mu_{B_{i-2}}(y), i = 3,4. \tag{4}$$

The membership function is the generalized bell function.

$$\mu_{A_i}(x) = \frac{1}{1 + \left[\left(\frac{x - c_i}{d_i} \right)^2 \right]^{b_i}} \tag{5}$$

Where {b_i, c_i, d_i} is the parameter set referred to as premise parameters.

Layer 2: Inference layer or rule layer

$$O_{2,i} = \omega_i = \mu_{A_i}(x) \times \mu_{B_i}(y), i = 1,2. \tag{6}$$

Firing strength ω_i is generated with product method.

Layer 3: Implication layer

$$O_{3,i} = \omega_i \circ C_i, i = 1,2. \tag{7}$$

Implication operator is product.

Layer 4: Aggregation layer

$$O_4 = \sum \omega_i \circ C_i, i = 1,2. \tag{8}$$

Aggregate operator is sum. The consequent parameters are determined by C_i. If the consequent MF is trapezoidal membership function, each MF has 4 nonlinear parameters to be adjusted.

Layer 5: defuzzification layer

$$O_5 = D \circ O_4 \tag{9}$$

$$U_{\text{Design}}(\text{COA}) = \frac{\sum_{i=0}^n \mu_{\text{Design}} \cdot z}{\sum_{i=0}^n \mu_{\text{Design}}}$$

The crisp output f is achieved with the defuzzification method, COA (center of area). {b_i, c_i, d_i} are premise parameters. The type of membership functions (MF) of the inputs are generalized bell functions, each MF has 3 nonlinear parameters. If the consequent MF is trapezoidal membership function, then each MF has 4 nonlinear parameters to be adjusted. Total nonlinear parameters in this example are 20. When there is adequate training data, we can achieve M-ANFIS model. We can also test the M model by checking data.

Weight Updating Formula

Weight updating formulas are very important for adjusting M-ANFIS model parameters. In this section, we conclude the weight updating formula for M-ANFIS model by discussing the general weight updating formula based on basic idea of back propagation in NN. An adaptive network is a network structure whose overall input-output behavior is determined by a collection of modifiable parameters (Yang et al 2000). A feed forward adaptive network is a static mapping between its inputs and output spaces. Our goal is to construct a network for achieving a desired nonlinear mapping. This nonlinear mapping is regulated by a data set consisting of desired input-output pairs of a target system to be modeled: this data set is called training data set. The procedures that adjust the parameters to improve the network's performance are called the learning rules. A learning rule explains how these parameters (or weights) should be updated to minimize a predefined error measure. The error measure computes the discrepancy between the network's actual output and a desired output (Yuanyuan et al 2009). The steepest descent method is used as a basic learning rule. It is also called back-propagation (Cheng et al., 1993). Our task is to minimize an overall error measure defined as:

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$$E_p = \sum_{k=1}^N (d_k - x_{l,k})^2 \tag{10}$$

Where, d_k is the k^{th} component of the p^{th} desired output vector and $x_{l,k}$ is the k^{th} component of the predicted output vector produced by presenting the p^{th} input vector to the network.

The general weight-updating formula is

$$\Delta\omega_{ji} = -\eta(d_i - x_i) \cdot x_j \cdot X \tag{11}$$

Where, η is the learning step, d_i is the desired output for node i , x_i is the real output for node i , x_j is the input for node i , X is a Polynomial, usually $(x_i \times (1 - x_i))$.

III. MODELING OF HEAT EXCHANGER USING M-ANFIS

In order to verify the validity of M-ANFIS model of heat exchanger presented in this paper, we apply this M-ANFIS into the evaluation U_{Design} of heat exchanger. Through training and testing this model by historical sample data, the results indicate that this model has ability of mapping heat exchange input data to the value of overall heat transfer coefficient designed U_{Design} . In the mean time, it is illuminated that M-ANFIS model shows great superiority to ANFIS model according to the experiments results analysis between them. Sample data in this experiment are supported by power plant expert engineers. All these data are obtained by experts confirm and are reliable.

Overall heat transfer coefficient Designed U_{Design} Evaluation

In heat exchanger system, U_{Design} is a quality measure describing operational conditions within a system. Now a day in power plant evaluation of U_{Design} is a fundamental factor for reliable performance decision-making. Basic sensor data (such as T_{hi} - hot water inlet temperature, flow rate of cold water F_{ci} and flow rate of hot water F_{hi}) are obtained by detector and are effective for U_{Design} synthetic evaluation. All these data are divided into training data and testing data. According to potential mapping relation between U_{Design} and those three indices, we apply this M-ANFIS to U_{Design} evaluation. Consequently, experiments by these sample data shows that the M-ANFIS model introduced in this paper provide theoretical basis and a new methodology for multi-inputs synthetic U_{Design} evaluating.

M-ANFIS model

In ANFIS, the output of each rule is a linear combination of input variables plus a constant term, and the final output is the weighted average of each rule's output. U_{Design} reflects the operator's subjective feelings on the heat exchanger; obviously the above model can't reflect the true nature of U_{Design} because of its linear output. M-ANFIS model is able to resolve this issue because grades of U_{Design} in consequent part are expressed as membership function rather than a simple linear equation. M model reflects the true meaning of U_{Design} and logic reasoning of operator. In Fig.3, the evaluating process of U_{Design} is illustrated. Consequently, we construct the following model. See in Fig.4. In this model, x, y, z represents the input, which is T_{hi}, F_{ci} and F_{hi} . A_1-A_3 represents membership functions of T_{hi} ; B_1-B_3 represents membership functions of F_{ci} ; C_1-C_3

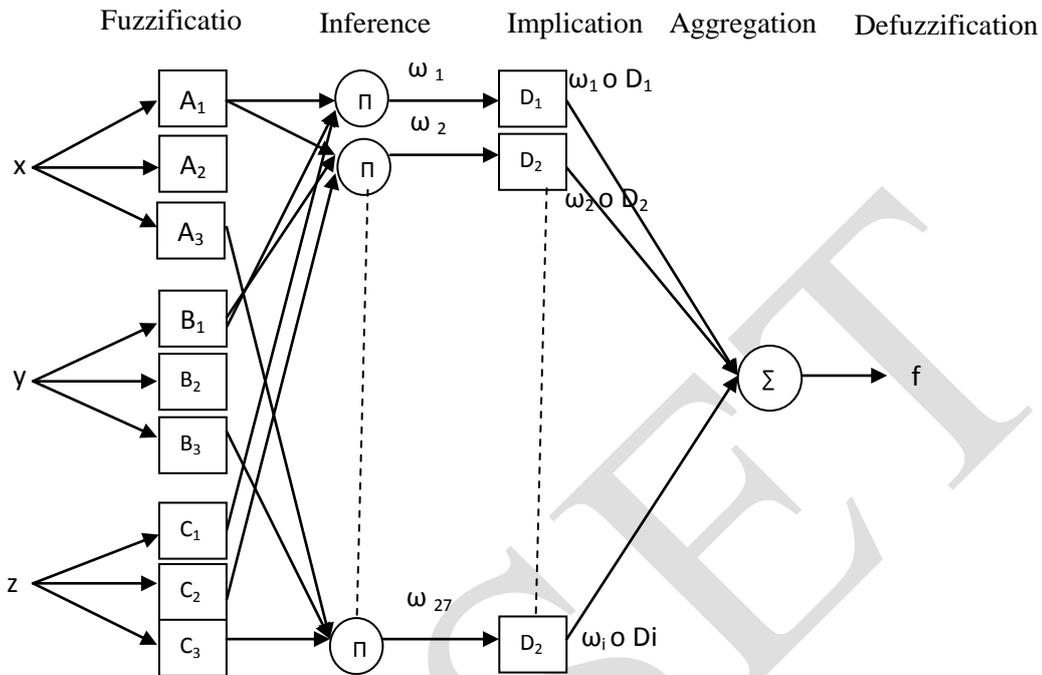


Fig.2 Structure of M-ANFIS for U_{Design} Evaluation

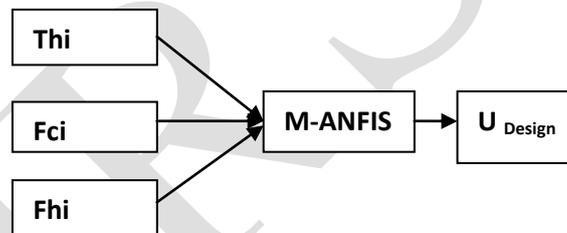


Fig.3 Process of Mamdani ANFIS for U_{Design} Evaluation

represents membership functions of F_{hi} . D_1 - D_6 represents membership functions of U_{Design} output. Rule's format is:

Rule 1: If x is A_1 and y is B_1 and z is C_1 , then $U_{Design} = A$.

In this model, premise parameters are 27 and consequent parameters are 24, which are all nonlinear parameters. We adjust all these parameters in M-ANFIS based on the weights updating formula, which is shown in Eq.16 and Eq.17.

All procedures are implemented with Matlab 7.1. The experiment on evaluating U_{Design} chooses 2000 pairs sample data (1500 pairs for training and 500 for testing).

The training process takes 0.55 second and 500 steps. The mean square error is 0.0003. The training errors are shown in Fig.6. The desired output and real output of M-ANFIS are in Fig.7. Testing errors are in Fig.8. Average test error is 0.0412. Indices of ANFIS and M-ANFIS are in Table 1. From this table, we can conclude that M-ANFIS model is superior to ANFIS in amount of adjusted parameters, scale of training data, consume time and testing error. Training error satisfies

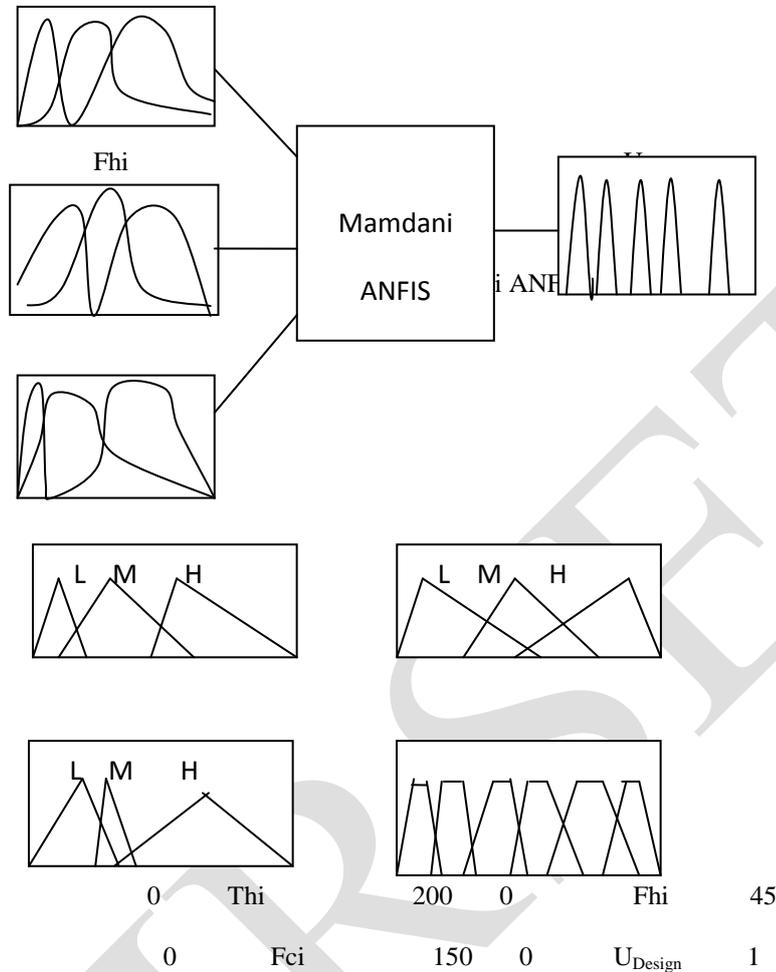


Fig.5 MFs of inputs and output after training

the requirements. It is clear that M-ANFIS is more effective subject to small-scale sample data. In the experiment, M-ANFIS, with 6 MFs in the consequent part, reflect the essence of U_{Design} precisely.

Table 1 Comparison between M-ANFIS and ANFIS

	M-ANFIS	ANFIS
Parameter Number	45	150
Training Steps	500	1500
Training Error	0.0003	8.558 e-006
Testing Error	0.0412	0.0897
Time Taken in Seconds	0.55	8.45

IV. EXPERIMENTAL SET-UP

Experiments are conducted on a 1-1 shell and tube heat exchanger. Cold and hot water flow into the shell and tubes respectively can be changed using pneumatic control valves. The inlet flow of the cold water can be varied in the range of 0 - 400 liter per hour (LPH) and that of hot water between 0 and 300 LPH. The flow rate of cold and hot water were measured using flow transmitter. In experimental design, three levels of process parameters hot water inlet temperature,

cold water flow rate and hot water flow rate were selected and are tabulated in Table 2. In this study, full factorial design of experiments is used and their experimental combinations of process parameters were presented in Table 3. The overhead tank water temperature is set initially as 45°C, cold water flow rate as 150 LPH and hot water flow rate as 70 LPH. In this set condition, the process was continued until it reaches the steady state. In steady state, the outlet temperatures of cold and hot water are observed. The flow rate of cold water was changed to 250 LPH and 350 LPH and continues the process to reach steady state. Then the outlet temperatures of cold and hot water were observed. The above step can be repeated by changing the hot water flow rate to 80 LPH and 90 LPH and the outlet temperatures were observed. Similarly for the hot water inlet temperature

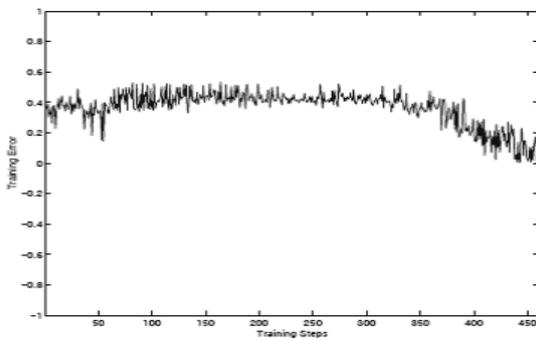


Fig.6 Training error

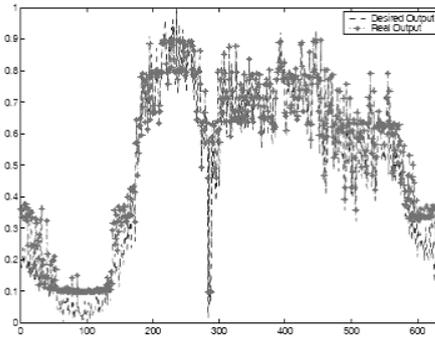


Fig.7 Desired and real output

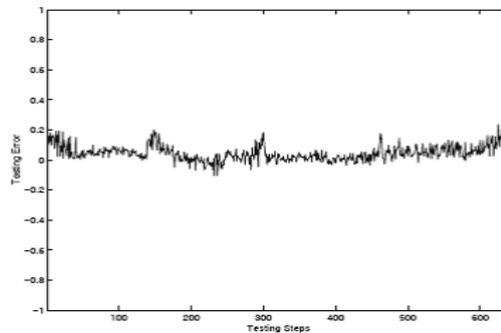


Fig.8 Testing error

55°C and 65°C the above procedure was repeated and the readings were observed. Based on the experimental design combination experiments were conducted for water – hot water system and their results are tabulated in the Table 3. The performance of the heat exchanger is assessed by computing overall heat transfer coefficient. The overall heat transfer coefficient is calculated using log mean temperature difference (LMTD) approach because the inlet temperature, outlet temperature and flow rate of the cold and hot water are known. The overall heat transfer coefficient of shell and tube heat exchanger is calculated by using below equations.

$$Q_h = m_h C_{ph} (T_{hi} - T_{ho}) \text{ in kW} \tag{12}$$

$$\text{(or)} \quad Q_c = m_c C_{pc} (T_{co} - T_{ci}) \text{ in kW} \tag{13}$$

Where Q_h - heat transfer rate of hot water side, Q_c - heat transfer rate of cold water side, m_h - mass flow rate of hot water in kg/hr, m_c - mass flow rate of cold water in kg/hr, C_{ph} – specific heat capacity of hot water in kJ/kgK, C_{pc} – specific heat capacity of hot water in kJ/kgK, T_{hi} – hot water inlet temperature in °C, T_{ho} - hot water outlet temperature in °C, T_{co} - cold water inlet temperature in °C, T_{ci} - cold water outlet temperature in °C, A - Heat transfer Area in m^2

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Table 2. Selected parameters and their levels

Input Parameter	Unit	Level 1	Level 2	Level 3
F _{ci} -Cold water Flow rate	LPH	150	250	350
F _{hi} -Hot water Flow rate	LPH	70	80	90
T _{hi} -Hot water inlet temperature	°C	45	55	65

LPH = Liter per hour

$$\text{Capacity ratio } R = (T_{hi} - T_{ho}) / (T_{co} - T_{ci}) \tag{14}$$

$$\text{Effectiveness } S = (T_{co} - T_{ci}) / (T_{hi} - T_{ci}) \tag{15}$$

F - Correction factor for LMTD to account cross flow

$$F = [(R+1)1/2 \times \ln((1-SR)/(1-S))] / (1-R) \times \ln\{[2-S(R+1-(R-1)1/2)] / [2-S(R+1+(R+1)1/2)]\} \tag{16}$$

$$\text{LMTD for Counter current flow} = ((T_{hi} - T_{co}) - (T_{ho} - T_{ci})) / \ln((T_{hi} - T_{co}) / (T_{ho} - T_{ci})) \text{ in } ^\circ\text{C} \tag{17}$$

$$\text{LMTD for Co current flow} = ((T_{hi} - T_{ci}) - (T_{ho} - T_{co})) / \ln((T_{hi} - T_{ci}) / (T_{ho} - T_{co})) \text{ in } ^\circ\text{C} \tag{18}$$

$$U = [Q_h \text{ or } Q_c] / [A * F * \text{LMTD}] \text{ in } \text{kW/m}^2\text{ } ^\circ\text{C} \tag{19}$$

Table 3. Experimental design using full factorial design of experiments and their outputs

Ex. No.	T _{hi} (°C)	F _{hi} (LPH)	F _{ci} (LPH)	Experimental observation	
				T _{co} (°C)	T _{ho} (°C)
1	45	70	150	33	34.5
2	45	70	250	32.5	34
3	45	70	350	32	33.5
4	45	80	150	33.75	34.5
5	45	80	250	33.25	35
6	45	80	350	32.75	34.5
7	45	90	150	33.25	36.75
8	45	90	250	33	35.5
9	45	90	350	32.25	35

V. DESIGN AND DEVELOPMENT OF PERFORMANCE ASSESSMENT SYSTEM FOR HEAT EXCHANGER

Design of performance assessment system

A monitoring system for shell and tube heat exchanger was designed based on the current need to evaluate the performance. In this an M-ANFIS is used to develop the model for predicting the overall heat transfer coefficient (U_{Design}) of the design system using secondary measurements temperature and flow rates. Inputs of the developed network were Thi- hot water inlet temperature , flow rate of cold water Fci and flow rate of hot water Fhi and output was U_{Design}. Data acquired from the design of experiments were used for training, validation and testing the M-ANFIS model. Heat transfer coefficient of real system (U_{Real}) is derived using secondary measurements such as T_{ci}, T_{hi}, T_{co}, T_{ho}, F_{ci} and F_{hi}. This system imitate the real time system and used for performance assessment (fouling) of the system. Measured values of T_{ci}, T_{hi}, T_{co}, T_{ho}, F_{ci} and F_{hi} are used to predict the value of U_{Design} and compute the value of U_{Real}. FF value is computed with the predicted value of U_{Design} and the computed value of U_{Real}. It is used to identify the performance degradation or degree of fouling of the heat exchanger. If the FF value is greater than or equal to the set value (allowable) of design heat exchanger, warning message will be given for cleaning or maintenance of heat exchanger and the heat exchanger continue to work and monitor the system. Otherwise no warning message will be given and the heat exchanger continues to work and monitor the system. The proposed scheme and flow chart of the online performance monitoring system is shown in Fig.9.

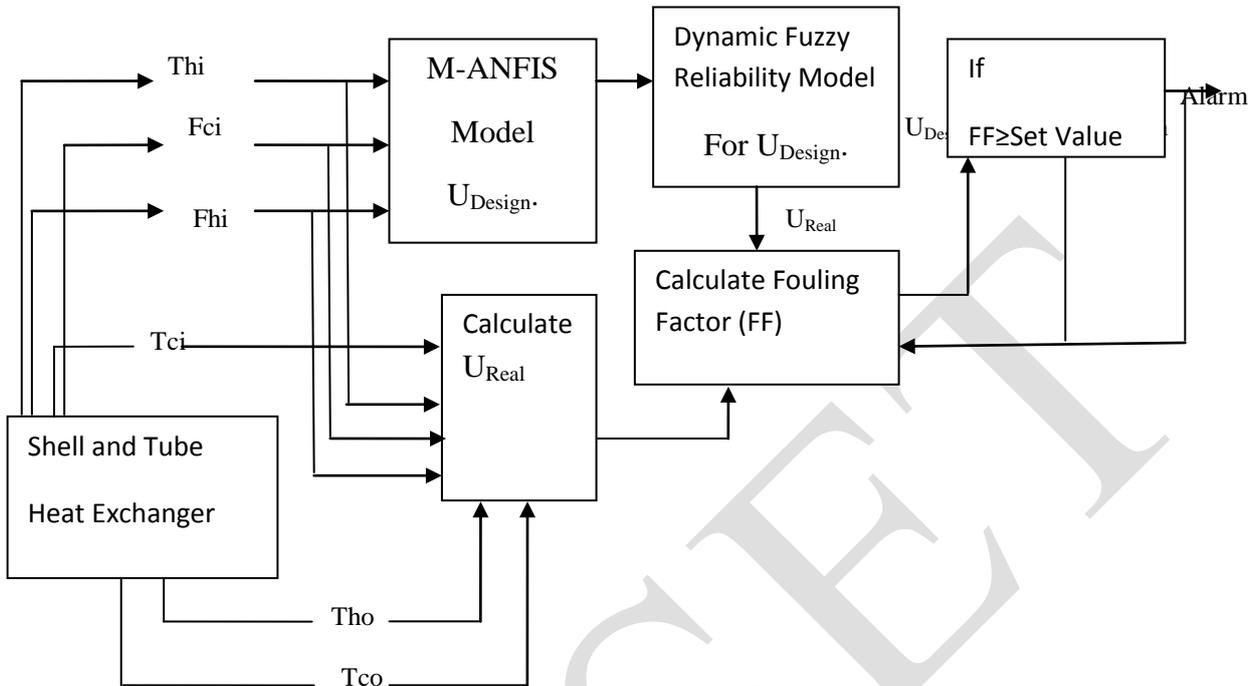


Fig. 9 Schematic diagram of proposed performance monitoring system

M-ANFIS model development

Thi, Fci and Fhi and one neuron in the output layer, corresponding to the process response U_{Design} . The topography of the M-ANFIS model for U_{Design} is shown in Fig.2. and the developed model in MATLAB environment is shown in Fig.3.

Table 4. Heat transfer rate (Qh) and overall heat transfer coefficient (U) of experimental data

Ex. No	Qh (kW)	A*F*LMTD (m ² .°C)	U_{Design} (kW/m ² .°C)
1	0.4114	2.0791	0.1721
2	0.4491	2.1176	0.1843
3	0.4867	2.1640	0.1954
4	0.4041	2.1901	0.1576
5	0.4375	2.0480	0.1851
6	0.4809	2.0791	0.2001
7	0.3536	2.8124	0.1206
8	0.4174	2.4381	0.1607
9	0.4966	2.4601	0.1772

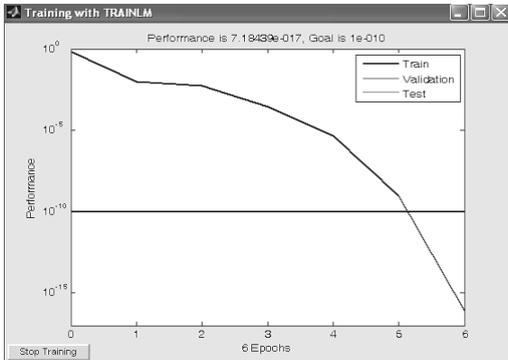


Fig.10 Training graph of developed M-ANFIS model for U_{Desi}

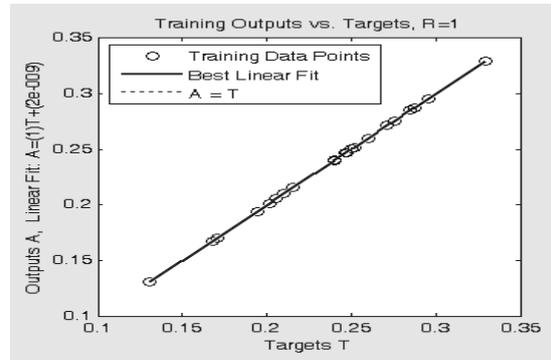


Fig.11 Training Output value graph of developed M-ANFIS model for U_{Design}

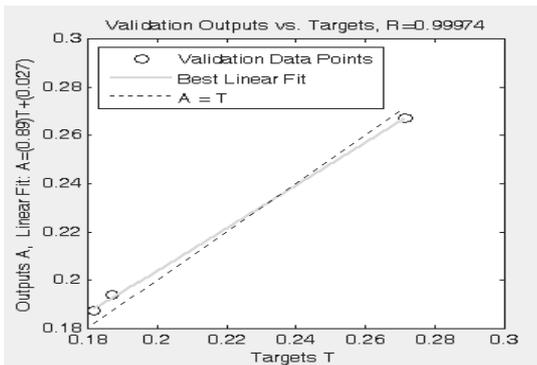


Fig.12. Validation Output value graph of developed M- ANFIS model for U_{Design}

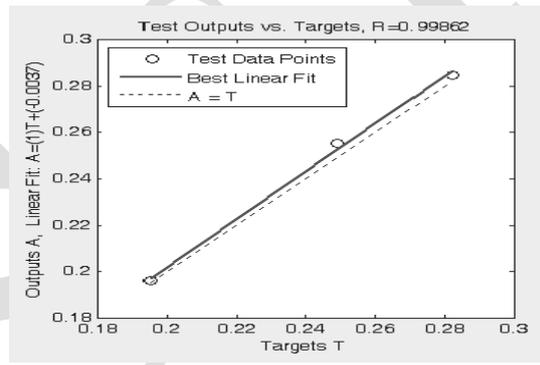


Fig.13 Testing Output value developed M-ANFIS model for

Experimental data set are used to train, validate and test the U_{Design} network. The variation of MSE during the training is shown in Fig.10. The graphical output of M-ANFIS is shown in Fig.13 for U_{Design} .

It is observed that predicted values of U_{Design} are very closer to the actual values that are shown in Fig.12. It is also found that maximum absolute error of U_{Design} is 3.46 % is tabulated in Table 4. This indicates that the model accuracy for predicting the process responses is well adequate. For testing, other three new data set are used which do not belong to the training and validation data set. For this testing data set, the overall heat transfer coefficient is predicted using the M-ANFIS model and then compared with the actual values. It is observed that predicted values of U_{Design} are very closer to the actual values that are shown in Fig.13. It is also found that maximum absolute error of U_{Design} is 2.54 % is presented in Table 6.

Table 5. Experimental results vs M-ANFIS prediction results for validation

T_{hi} °C	F_{hi} LPH	F_{ci} LPH	T_{co} °C	T_{ho} °C	U_{Design} (kW/m ² .°C)		% Error
					Actual value	M-ANFIS	
45	70	150	33.5	35	0.1721	0.1772	2.79
45	90	350	33.75	35.75	0.1772	0.1837	3.46
55	90	250	35.25	37.75	0.2615	0.2573	1.66

Table 6. Experimental results v/s M-ANFIS prediction results for testing data

T _{hi} °C	F _{hi} LPH	F _{ci} LPH	T _{co} °C	T _{ho} °C	U _{Design} (kW/m ² .°C)		% Error
					Actual value	M-ANFIS	
45	80	250	33.5	34	0.1851	0.1861	0.49
55	80	150	35	36.5	0.2391	0.2454	2.54
65	80	350	37	38.5	0.2720	0.2748	0.97

This indicates that the model for predicting the process responses is well adequate for generalization. M-ANFIS model for U_{Design} is developed to study the performance degradation by estimating the fouling of the shell and tube heat exchanger.

Performance assessment

Effective and majorly applied method for fouling detection is to compare the U_{Design} and U_{Real}. It cannot be measured directly and it uses the secondary measurements such as flow rates and temperatures as inputs from the experimental data to estimate it. From the online measured values such as T_{ci}, T_{hi}, T_{co}, T_{ho}, F_{ci} and F_{hi} the performance of the heat exchanger is assessed. T_{hi}, F_{ci} and F_{hi} were used to predict the value of U_{Design} using developed M-ANFIS model. The consequent part of M-ANFIS is fuzzy in nature and its defuzzyfication gives the crisp value of U_{Design}. U_{Real} value is computed using LMTD approach with T_{ci}, T_{hi}, T_{co}, T_{ho}, F_{ci} and F_{hi}. The performance of heat exchanger is assessed by comparing the U_{Real} value with U_{Design} value. The decrease in U_{Real} value indicates the degradation of performance by formation of fouling. In this, performance degradation or fouling is estimated using FF approach and this will indicate the degree of fouling. The degradation in performance is expressed by the FF, as calculated by the equation:

$$FF = [(1/U_{Real}) - (1/U_{Design})] \tag{20}$$

Here

U_{Design} is predicted using M-ANFIS model with T_{hi}, F_{ci} and F_{hi}.

U_{Real} value is computed using LMTD approach with T_{ci}, T_{hi}, T_{co}, T_{ho}, F_{ci} and F_{hi}.

The FF value of heat exchanger is calculated using the equation (21). In design stage, the allowable fouling resistance i.e. FF is specified for all the heat exchangers by manufacturer's to avoid frequent cleaning or maintenance. The tolerance value of FF is obtained from the specification or from the data book. If the estimated FF value is greater than or equal to set value of FF, it gives warning message for cleaning or maintenance and continues the operation. Otherwise, no warning message is given and the operation continues.

VI. DYNAMIC FUZZY RELIABILITY MODELING

The success and failure are treated as fuzzy events, which contains continuous performance characteristic values exhibiting different degrees of success or failure. The dynamic fuzzy reliability of a component depends on time and it can be evaluated as the probability of the fuzzy event of success (Zadeh, 1968). Thus fuzzy reliability is defined as:

$$R_{SUDesign} = Pr [\text{fuzzy success}] = \int \mu_{SUDesign}(y) dF(y(t) = E[\mu_{SUDesign}(Y)]) \tag{21}$$

Similarly Fuzzy unreliability is defined in terms of the fuzzy failure event as:

$$R_{FUDesign} = Pr [\text{fuzzy failure}] = \int \mu_{FUDesign}(y) dF(y(t) = E[\mu_{FUDesign}(Y)]) \tag{22}$$

$\mu_{FUDesign}(y) = 1 - \mu_{SUDesign}(y)$, and E [μ_{SUDesign}(Y)] is a function of time.

μ_{SUDesign} = Membership function of overall heat transfer coefficient (U_{Design}) for success

μ_{FUDesign} = Membership function of overall heat transfer coefficient (U_{Design}) for failure

where F(y(t)) is the cumulative distribution function of the performance characteristic variable at a given time point. The fuzzy reliability definition degenerates to the classic binary reliability model when the membership function of fuzzy success event is substituted with the characteristic function of a crisp success event. This fuzzy reliability definition is also an analog to the system's performance measure based on the state expectation definition given by $E[X] = \sum_{i=0}^M i * Pr[X = i]$, which has been traditionally used for both binary and multi-state reliability modeling (Russell and Kapur, 1997).

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VII. RESULTS AND DISCUSSION

The proposed performance monitoring scheme is implemented in the developed experimental setup located in the process lab. The data of heat exchanger such as T_{ci} , T_{co} , T_{hi} , T_{ho} , F_{ci} and F_{hi} are captured by running the MATLAB program in PC, which is connected to the data acquisition system. The system initially predicts the U_{Design} value with M-ANFIS model and dynamic fuzzy reliability model and computes the U_{Real} value through the experimental observed values. The dynamic reliability for success and failure events of U_{Design} are calculated using dynamic reliability modeling formulae. Then the system computed the FF value using U_{Real} and U_{Design} values. Based on the FF value the system gives the information to the operator. The results of the system for typical condition are shown in table 6. Here for $FF < Set\ FF = Not\ Alarming$, and for $FF > Set\ FF = Alarming$.

Table7. FF Calculation

S.No	U_{Design} By M-ANFIS & Fuzzy Reliability model	U_{Real}	$1/U_{Design}$	$1/U_{Real}$	$FF=(5)-(4)$	Set FF (Allowable)	Alarm Condition
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
1	0.1721	0.17209	58.1057	58.1079	0.0022	0.0025	Not Alarming
2	0.1843	0.18428	54.2593	54.2631	0.0038	0.0025	Alarming
3	0.1954	0.19538	51.1770	51.1799	0.0029	0.0025	Alarming
4	0.1576	0.15759	63.4517	63.4530	0.0013	0.0025	Not Alarming
5	0.1851	0.18509	54.0248	54.0267	0.0019	0.0025	Not Alarming
6	0.2001	0.20008	49.9750	49.9782	0.0032	0.0025	Alarming
7	0.1206	0.12059	82.9187	82.9238	0.0051	0.0025	Alarming
8	0.1607	0.16069	62.2277	62.2285	0.0008	0.0025	Not Alarming
9	0.1772	0.17719	56.4334	56.4351	0.0017	0.0025	Not Alarming
10	0.2368	0.23677	42.2297	42.2333	0.0036	0.0025	Alarming
11	0.2417	0.24167	41.3736	41.3780	0.0044	0.0025	Alarming
12	0.2497	0.24966	40.0480	40.0542	0.0062	0.0025	Alarming
13	0.2391	0.23908	41.8235	41.8256	0.0021	0.0025	Not Alarming
14	0.2748	0.27478	36.3901	36.3925	0.0024	0.0025	Not Alarming
15	0.2853	0.28525	35.0508	35.0569	0.0061	0.0025	Alarming

From the results it is identified that the heat exchanger performance is within the tolerance value (set by field engineer/maintenance engineer) of FF. It shows no warning message to field engineers. Another typical condition results are shown in table 6. This inferred that the performance of the heat exchanger is above the tolerance value of FF. It needs immediate maintenance or corrective action to recover the heat transfer efficiency. This gives intimation to the operator for planning maintenance well ahead to minimize operational disturbance due to unplanned shutdowns.

VIII. CONCLUSION

ANFIS, introduced by R. Jang, is the most popular one. In the process of fuzzy inference, ANFIS adopts a linear equation in consequent part, which cannot exhibit human's judgment reasonably. So, we propose the Mamdani model based adaptive fuzzy inference system (M-ANFIS), which has greater superiority in consequent part and intuitive of fuzzy reasoning. M-ANFIS is a universal approximator because of its infinite approximating capability by training. All parameters in M-ANFIS are nonlinear parameters which can be adjusted by learning rules discussed above. M-ANFIS model can show its legibility and understandability and exhibit the essence of fuzzy logic more clearly. Finally, we use

International Journal of Innovative Research in Science, Engineering and Technology

(An ISO 3297: 2007 Certified Organization)

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M-ANFIS into Performance Assessment of Heat Exchanger. The experimental results show that M-ANFIS model is superior to ANFIS in amount of adjusted parameters, scale of training data, consume time and testing error. Experiments were conducted on a 1-1 shell and tube heat exchanger with different cold water flow rates, hot water flow rate, and hot water inlet temperature to assess the performance of the system. The experimental observations were incorporated into the M-ANFIS model development. A M-ANFIS model was developed to predict overall heat transfer coefficient U_{Design} of the design heat exchanger system and the model was trained, validated and tested for generalization. Good agreement was identified between the predictive model results and the experimental results. M-ANFIS model was used to predict the value U_{Design} and U_{Real} was derived from measured values. A dynamic fuzzy reliability model is proposed to evaluate the reliable value of U_{Design} for the reliable performance assessment of heat exchanger in terms of FF. It is shown that fuzzy modeling is more realistic for systems with continuous performance levels. FF is found from the predicted U_{Design} and U_{Real} value. From the estimated FF value, the performance degradation/fouling effect was within the tolerance limit (margin) or not is identified. Based on the results, degree of fouling and precaution information like warning or maintenance was given. Further, it needs intelligent approach to do fouling analysis and maintenance decision.

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