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Numerical Solution of Imbibition Phenomenon in a Slightly Dipping Porous Medium with Magnetic Fluid

N.S.Rabari¹, A.V.Patel², P.H. Bhathawala³

¹Assistant Professor, Mehsana Urban Institute of Sciences, Ganpat Vidyanagar-384012, Gujarat, India.

²Associate Professor, Pramukh Swami Science College, Kadi-382715, Gujarat, India

³Rtd.Professor & Head, Department of Mathematics, VNSG University, Surat – 394510, Gujarat, India

ABSTRACT: In this paper, we have discussed imbibition phenomenon in double phase flow through slightly dipping porous media. The mathematical formulation leads to non linear partial differential equation governing the phenomenon in a homogeneous medium with magnetic fluid. The mathematical solution has been obtained by finite element method with appropriate initial and boundary condition. Finite element method is a numerical method for finding an approximation solution of differential equation in finite region or domain. We obtained graphical representation of the solution using a Matlab coding.

KEYWORDS: Slightly dipping porous media, fluid flow, magnetic fluid, finite element method.

I. INTRODUCTION

It is well known that when a porous medium filled with some fluid is brought into contact with another fluid which preferentially wets the medium, there is a spontaneous flow of the wetting fluid into the medium and a counter flow of the resident fluid from the medium. Such a phenomena arising due to difference in wetting abilities is called countercurrent imbibition. These phenomena have been formally discussed by Brownscombe and Dyes [4], Enright [5], Braham and Richarson [6], Rijik [7], Rijik et al [9], for homogeneous porous medium.

II. STATEMENT OF THE PROBLEM

We consider the finite cylindrical piece of oil saturated porous matrix of length L (=1) is inclined at small angle θ with the horizontal. The present problem of linear counter current imbibition is furnished, when the three sides of the matrix are bounded by impermeable surfaces and the open end is exposed to liquid involving magnetic fluid (as in figure).

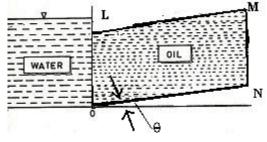


Figure 1.



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III. MATHEMATICAL FORMULATION OF THE PROBLEM

The equation of filtration velocity of injected liquid (w), becomes

$$V_{w} = -\left(\frac{K_{w}}{\delta_{w}}\right) K \left[\frac{\partial P_{w}}{\partial x} + \gamma H \frac{\partial H}{\partial x} + \rho_{w}g \sin\theta\right] \qquad \dots \dots \dots (1)$$

Where, $\gamma = \mu_o \lambda + \frac{16 \lambda \mu_o \lambda^2 r^3}{9(l+2)^3}$ and equation of velocity of native liquid (V_o) is

$$V_o = -\left(\frac{K_o}{\delta_o}\right) K \left[\frac{\partial P_o}{\partial x} + \rho_o g \sin\theta\right] \qquad \dots \dots \dots (2)$$

On simplifying equation (1) and equation (2) by using equation (3) and (4), we obtain

$$\frac{\partial p_{w}}{\partial x} = -\left[\frac{-K_{w}\delta_{o}\left[\gamma H\frac{\partial H}{\partial x} + \rho_{w}g\sin\theta\right] - K_{o}\delta_{w}\left[\frac{\partial P_{o}}{\partial x} + \rho_{o}g\sin\theta\right]}{\left(K_{o}/\delta_{o} + K_{w}/\delta_{w}\right)}\left[\frac{\partial P_{c}}{\partial x}\right]\right]$$

Substituting above equation into equation (1), we obtain

$$V_{w} = \frac{K K_{o} K_{w}}{\left(K_{o}/\delta_{o} + K_{w}/\delta_{w}\right)} \left[\frac{\partial P_{c}}{\partial x} - \gamma H \frac{\partial H}{\partial x} + \left(\rho_{o} - \rho_{w}\right)g\sin\theta\right]$$

Since, $\frac{K_o K_w}{K_o \delta_w + K_w \delta_o} \approx \frac{K_o}{\delta_o}$, Above equation reduces to the form

The equations of continuity of the two phases,

$$P\left(\frac{\partial S_{w}}{\partial t}\right) + \frac{\partial}{\partial x}\left(\frac{K K_{o}}{\delta_{o}}\left[\frac{\partial P_{c}}{\partial x} - \gamma H \frac{\partial H}{\partial x} + (\rho_{o} - \rho_{w})g\sin\theta\right]\right) = 0$$

For definiteness of the mathematical analysis, we assume standard relationship between phase saturation and relative permeability, above equation becomes,

$$P\left(\frac{\partial S_{w}}{\partial t}\right) + \frac{K}{\delta_{o}}\frac{\partial}{\partial x}\left(\left(1 - \alpha S_{w}\right)\left[-\beta_{o}\frac{\partial S_{w}}{\partial x} - \gamma H\frac{\partial H}{\partial x} + \left(\rho_{o} - \rho_{w}\right)g\sin\theta\right]\right) = 0 \qquad \dots \dots (6)$$

This is the desired non linear differential equation of motion which describes the linear counter current imbibition phenomena in a homogeneous porous medium with effect of magnetic fluid.



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Considering the magnetic fluid H in the x-direction only, we may write, $H = \frac{\Lambda}{r^n}$ where Λ is a constant parameter and n is an integer. Using the value of H for n = -1 in equation (6), we get,

where $C_1 = P$, $C_2 = \frac{K\rho_o}{\delta_o}$, $C_3 = \frac{\mu}{\delta_o}$, $C_4 = \frac{K}{\delta_o}(\rho_o - \rho_w)g\sin\theta$

A set of suitable boundary conditions,

 $S_{w}(x,0) = 0$

for all x > 0;(8)

$$S_w(0,t) = S_{w0}$$
; $S_w(L,t) = S_{w1}$ for all $t \ge 0$ (9)

Equation (7) is reduced to dimensionless form by setting,

Where $C_5 = \frac{-C_3 L^2 \alpha}{C_2}$, $C_6 = \frac{C_4 L \alpha}{C_2}$,

The initial and boundary conditions (8) & (9) now becomes,

$$\begin{split} S_w(x,0) &= 1 & \forall x > 0 & \dots \dots (11) \\ S_w(0,t) &= 1 - \alpha \, S_{w0} \ ; & S_w(L,t) &= 1 - \alpha S_{w1} & \text{ for all } t \geq 0 & \dots \dots (12) \end{split}$$

Equation (10) is desired nonlinear differential equation of motion for the flow of two immiscible liquids in homogeneous medium wit effect of magnetic fluid. A Matlab Code is prepared and executed with $C_5 = 4.046 \times 10^{-11}$, $C_6 = 0.001*1.11$; h = 1/15, k = 0.002223 for 225 time levels, $S_{w0} = 0.5$ and $S_{w1} = 0$. Curves indicating the behavior of Saturation of injected fluid with respect to various time period.

IV. FINITE ELEMENT METHOD

For the problem under consideration, the length variable x varies between 0 and L (figure 2(a)). This domain is divided in to set of linear elements (figure 2(b)).

x = 0

x = 1

Figure 2(a).



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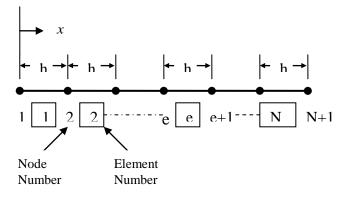


Figure 2(b).

Now, the variational form of given PDE is

Choose an arbitrary linear element $R^{(e)} = [S_1^{(e)}, S_2^{(e)}]$ & obtain interpolation function for $R^{(e)}$ using Lagrange interpolation Method such as

$$S^{(e)}(x) = \sum_{j=1}^{2} N_{j}(x) S_{j}^{(e)} = N^{(e)} \phi^{(e)} = \phi^{(e)^{T}} N^{(e)^{T}}$$
where
$$N^{(e)} = [N_{1} N_{2}] \quad \& \quad \phi^{(e)} = [S_{1} S_{2}]^{T}$$
.....(14)

and N_1 , N_2 are shape function for linear element.

Now, apply Variational Method to R^(e) therefore equation (13) becomes

: Equation 15 becomes



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For minimization, first differentiate equation (16) with respect to $\phi^{(e)}$

$$\frac{\partial J^{(e)}}{\partial \phi^{(e)}} = \int_{R^{(e)}} \left[N^{(e)} \phi^{(e)} \left(\frac{\partial N^{(e)^T}}{\partial x} \frac{\partial N^{(e)}}{\partial x} \right) \phi^{(e)} + 2 \left(N^{(e)^T} N^{(e)} \right) \frac{\partial \phi^{(e)}}{\partial t} + \left(C_5 x + C_6 \right) N^{(e)^T} \frac{\partial N^{(e)}}{\partial x} \phi^{(e)} \right] dx$$

Now, $\frac{\partial J^{(e)}}{\partial \phi^{(e)}} = 0$ \therefore The Element equation is

By Gauss Legendre Quadrature Method, we evaluate these integral. Thus, element matrix transform to

$$A^{(e)} = \int_{-1}^{1} \left(N^{(e)} N^{(e)} \right) Jdz \approx \sum_{I=1}^{r} A^{(e)} (z_I) W_I$$

$$B^{(e)}(\phi^{(e)}) = \int_{-1}^{1} N^{(e)} \phi^{(e)} \left(\frac{1}{J} \frac{\partial N^{(e)}}{\partial X} \frac{1}{J} \frac{\partial N^{(e)}}{\partial X} \right) Jdz \approx \sum_{I=1}^{r} B^{(e)} (z_I) W_I$$

$$C^{(e)} = \int_{-1}^{1} \left(C_5 \left(\frac{h}{2} (1+z_I) \right) + C_6 \right) \left(N^{(e)} \frac{1}{J} \frac{\partial N^{(e)}}{\partial z} \right) Jdz \approx \sum_{I=1}^{r} C^{(e)} (z_I) W_I$$

For $A^{(e)}$ and $C^{(e)}$, degree of polynomial p = 2 then r = 2 and For $B^{(e)}$, p = 1 then r = 1. z_I and W_I are corresponding gauss points and gauss weights with respect to 'r'. Then, the element matrix becomes,



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Assembling of elements: For a uniform mesh of N elements, by the equation (17) and equation (18), the assembled equation becomes, $A \frac{\partial \varphi}{\partial T} - B(\varphi)\varphi + C \quad \varphi + D \quad \varphi = 0$(19)

Equation (19) represents the assembled equation.

Time approximation: We have obtained the finite element equation in the global form, which represent a system of simultaneous ordinary differential equation. We introduced δ family of approximations which approximates weighted average of a dependent variable of two consecutive time steps by linear interpolation of the values of the variable at the



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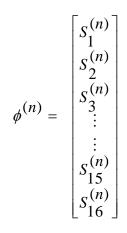
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0	0	0	:	:	$0 \dots \frac{2h}{3} - (1 - \delta) k \left(\frac{1}{2h} (S_1^{(n)}) + 2S_1^{(n)} + S_1^{(n)}) + \frac{C_5 h}{6} \right) \frac{h}{6} - (1 - \delta) k \left(\frac{1}{2h} (-S_1^{(n)}) - \frac{C_5 h}{3} - \frac{C_6}{3} \right)$	$0 \cdots \frac{h}{6} - (1 - \delta) \hbar \left(\frac{1}{2h} (-S_1^{(n)} - S_1^{(n)}) + \frac{G_5 h}{6} + \frac{G_6}{2} \right) - \frac{h}{6} - (1 - \delta) \hbar \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_5 h}{3} + \frac{G_6}{2} \right) = \frac{1}{6} - (1 - \delta) \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_5 h}{3} + \frac{G_6}{2} \right) = \frac{1}{6} - \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} + \frac{G_6 h}{2} \right) = \frac{1}{6} - \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} + \frac{G_6 h}{2} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} + \frac{G_6 h}{2} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} + \frac{G_6 h}{2} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} + \frac{G_6 h}{2} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac{1}{6} - \frac{1}{6} \left(\frac{1}{2h} (S_1^{(n)} + S_1^{(n)}) + \frac{G_6 h}{3} \right) = \frac{1}{6} - \frac$
o	0	0	÷	÷	$\frac{2\hbar}{3} - (1 - \delta) \hbar \left(\frac{1}{2\hbar} (S_1^{(\eta)} + 2S_1^{(\eta)} + S_1^{(\eta)} + S_1^{(\eta)}) + \frac{C_5\hbar}{6} \right)$	$\frac{h}{6} - (1 - \delta)\hbar \left(\frac{1}{2\hbar} (-S_1^{(\eta)} - S_1^{(\eta)}) + \frac{G_5 \hbar}{6} + \frac{G_6}{2} \right)$
		:	:	:		
o	$\frac{h}{6} - (1 - \delta)k \left(\frac{1}{2h} (-S_1^{(n)} - S_2^{(n)}) - \frac{C_5h}{3} - \frac{C_6}{2} \right)$	$\frac{\hbar}{6} - (1-\delta)\hbar \left(\frac{1}{2\hbar} (-S_2^{(\eta)} - S_3^{(\eta)}) + \frac{C_5\hbar}{6} + \frac{C_6}{2}\right) - \frac{2\hbar}{3} - (1-\delta)\hbar \left(\frac{1}{2\hbar} (S_2^{(\eta)} + 2S_3^{(\eta)} + S_4^{(\eta)}) + \frac{C_5\hbar}{6}\right) \cdots$	÷	:	o	0
$\frac{\hbar}{6} - (1 - \delta)\hbar \left(\frac{1}{2\hbar} (-S_1^{(1)}) - S_2^{(1)}) - \frac{C_5\hbar}{3} - \frac{C_6}{2}\right)$	$\frac{2h}{3} - (1-\delta)k \left(\frac{1}{2h}(S_1^{(n)} + 2S_2^{(n)} + S_3^{(n)}) + \frac{C_5h}{6}\right) - \frac{h}{6} - (1-\delta)k \left(\frac{1}{2h}(-S_1^{(n)} - S_2^{(n)}) - \frac{C_5h}{3} - \frac{C_6}{2}\right)$	$\frac{h}{6} - (1 - \delta)h\left(\frac{1}{2h}(-S_2^{(h)} - S_3^{(h)}) + \frac{C_5h}{6} + \frac{C_6}{2}\right)$	÷	÷	0	0
$\left[\frac{\mu}{3} - (1-\delta) k \left(\frac{1}{2h} (S_1^{(n)} + S_2^{(n)}) - \frac{C_5h}{6} - \frac{C_6}{2}\right)\right]$	$\frac{h}{6} - (1 - \delta)k \left(\frac{1}{2h}(-S_1^{(n)} - S_2^{(n)}) + \frac{C_2h}{6} + \frac{C_6}{2}\right)$	0	:	:	0	0



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$$\begin{split} F(\phi^{(n)}) = \\ \begin{bmatrix} \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(S_{1}^{(n)} + S_{2}^{(n)}) - \frac{C_{5}h}{6} - \frac{C_{6}}{2}\right)S_{1}^{(n)} + \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{1}^{(n)} - S_{2}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{2}^{(n)} \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{1}^{(n)} - S_{2}^{(n)}) + \frac{C_{5}h}{6} + |\frac{C_{6}}{2}\right)S_{1}^{(n)} + \frac{2h}{3} - (1-\delta)k\left(\frac{1}{2h}(S_{1}^{(n)} + 2S_{2}^{(n)} + S_{3}^{(n)}) + \frac{C_{5}h}{6}\right)S_{2}^{(n)} + \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{2}^{(n)} - S_{3}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{3}^{(n)} \\ & \vdots \\ \frac{2h}{3} - (1-\delta)k\left(\frac{1}{2h}(S_{14}^{(n)} + 2S_{15}^{(n)} + S_{16}^{(n)}) + \frac{C_{5}h}{6}\right)S_{15}^{(n)} + \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) - \frac{C_{5}h}{3} - \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{3} + \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{h}{3} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{3} + \frac{C_{6}}{2}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{5}h}{6} + \frac{C_{6}}{2}\right)S_{15}^{(n)} + \frac{C_{6}h}{3} - \frac{C_{6}h}{3} + \frac{C_{6}h}{3}\right)S_{16}^{(n)} \\ & & \vdots \\ \frac{h}{6} - (1-\delta)k\left(\frac{1}{2h}(-S_{15}^{(n)} - S_{16}^{(n)}) + \frac{C_{6}h}{3} + \frac{C_{6$$

where K is called global stiffness matrix and F is called global generalized force vector and N+1 is total number of global nodes .

Imposing boundary conditions: We now apply the boundary condition (12) to the global equation (24) of the problem and simplifying, we get



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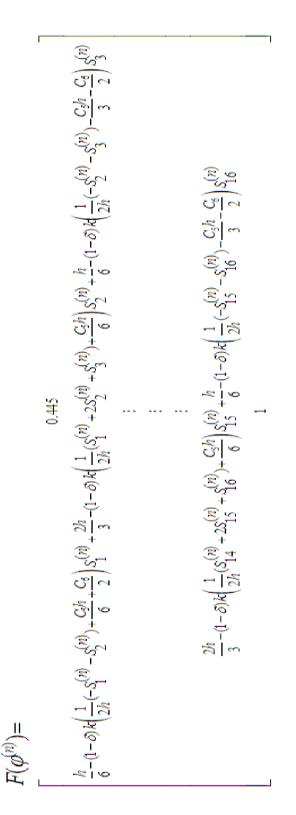
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Where,





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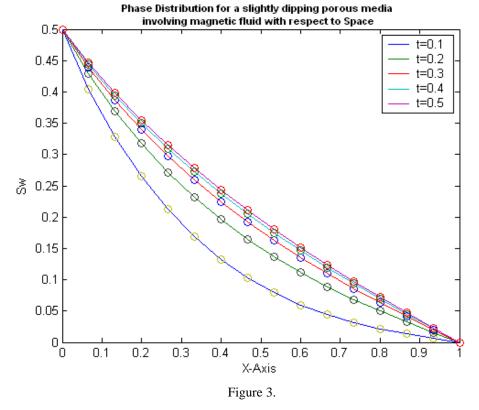
Thus, equation (25) is the resulting system of nonlinear algebraic equation. **Solution of nonlinear algebraic equation:** In the previous section, we obtained the assembled equation which is nonlinear. The assembled nonlinear equations after imposing boundary conditions are given by equation (25). We seek an approximate solution by the linearization which based on scheme

$$K(\phi^{(n)}) \phi^{(n+1)} = F$$
(26)

where $\phi^{(n)}$ denotes the solution of the n iteration. Thus, the coefficient K_{ij} are evaluated using the solution $\phi^{(n)}$ from the previous iteration and the solution at the $(n+1)^{th}$ iteration can be obtained by solving equation (26) using Gauss Elimination Method. At the beginning of the iteration (i.e. n=0), we assume the solution $\phi^{(0)}$ from initial condition which requires to have $S_1^{(0)} = S_2^{(0)} = \dots = S_{N+1}^{(0)} = 1$.

V. GRAPHICAL REPRESENTATION AND CONCLUSION:

A Matlab Code is prepared for 15 elements model and resulting equation (26) for N = 15 is solved by Gauss Elimination method.



In above graph, solution obtained with $C_5 = 4.046 \times 10^{-11}$, $C_6 = 0.001*1.11$; h = 1/15, k = 0.002223 for 225 time levels. It is clear from graph that $S_w = S_0(=0.5)$ at layer x = 0& there is no saturation of injected liquid at other end (x = 1) irrespective of time. At particular time, saturation of injected liquid involving magnetic fluid decrease with increase in value of x(or as we move ahead) and at x = 1, saturation is decreased to zero and as time increases, rate of increases of the saturation of injected liquid decreases at each layer.



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