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# Design and Analysis of Boom Structure of a Backhoe Loader

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**ABSTRACT:** With the increased requirement of accuracy of pay loads, the stiffness characteristics of structure are increasingly influencing the design and performance of a backhoe loader. The main objective of structural design is to achieve the minimum mass structure, which will satisfy the stiffness, strength and other requirements. Hence optimum configuration and advanced technology have to be incorporated to achieve minimum mass. In this study, static structural analysis of backhoe-loader arms has been performed with the finite element method (FEM). The aim of this study is to simulate and strengthen the back and front arms of the backhoe-loader concerning with stress under maximum loading condition and different boundary conditions. According to analysis result, back and front arms of the backhoe-loader are strengthened with the use of reinforcements. As a result of the study, strength of the arms has been increased by nearly 20%.

**KEYWORDS:** Design and Analysis.

## I. INTRODUCTION



Fig: 1.1 Backhoe-Loader

Backhoe-loader is a mobile machine which digs, elevates, loads and swings materials by the action of its mechanism consisting of backhoe and loader parts Backhoe-loader parts such as boom, arm, and loader arm limit the life expectancy of the backhoe loader. Therefore, backhoe loader parts must be strong enough to cope with caustic working conditions. It can be concluded that, strength analysis is an important step in the design of backhoe loader parts. Finite element analysis (FEA) is the most powerful technique in the strength calculations of the structures working under known loads and boundary conditions. These analyses show the critical points of the design early and so one can



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improve the design before producing prototypes. The analysis has been carried out using ANSYS Workbench finite element packet program. Maximum stress locations and reinforcement were both determined and applied. Strength of the arms has been increased after improvements.

#### II. RELATED WORK

#### 2.1 PROBLEM DESCRIPTION

Finite element analysis is a word used in recent language of Mechanical Engineer in which the problems are solved with the use of software using Finite element method to solve the difficult problems where the direct implication of the problem is not always ready in the formula's provided in the standards or the books. The Finite element method is a numerical procedure which can be used to solve numerical problems in Engineering. An unsophisticated description of the FE method is that it involves cutting a structure into several elements (pieces of the structure), describing the behaviour of each element in a simple way, than reconnecting elements at "nodes" as if nodes were pins or drops of glue that holds together the elements. This process results in the set of simultaneous algebraic equations which can be solved with mathematical formulations for solving the problem for deflection which can be further solved to get the results of strains and stresses. There may be several and thousands of such equations formed which means the computer implication is mandatory. A more sophisticated description of the FE method regards it as piecewise polynomial interpolation. That is over an element a field quantity such as displacement is interpolated from values of the field quantity at nodes.

#### 2.2 DESIGN CRITERIA

Assumptions used in the analysis are:

- Material behavior is linear elastic and strains are small. Therefore, linear elastic analysis will be carried out.
- Pins and links are assumed as rigid.
- The loads are applied statically
- Material properties of structures after heat treatment (welding operation) are not changing.

According to loader and bucket cylinder maximum pressure, breakout forces  $(W_{bf})$  were calculated using free body diagrams, Maximum breakout force was obtained and it was used in the analysis of the front arm with two different boundary conditions.

#### 2.3 AIM AND SCOPE OF THE PROJECT

To find the deformation and stress developed and verify the design of the Boom of backhoe loader for the given conditions.

This project work is mainly carried out for satisfying the following objectives:

- Conduct various case studies for finalizing the design of boom
- Carry out static analysic and extract the maximum stresses, strains, margin of safety and maximum displacement for the loads.
- The modeling and analysis carried out for the manufacturing of the rear chassis using THE CATIA V5 AND ANSYS11 software



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#### III. DESIGN AND FE ANALYSIS OF BOOM STRUCTURE OF A BACKHOE LOADER

#### **3.1 MODEL DESCRIPTION:**

The boom of Backhoe loader assembly is shown in the figure The Boom swinger connected to the rear chassis and the other end is connected to the arm. It is also connected to the lift cylinder.

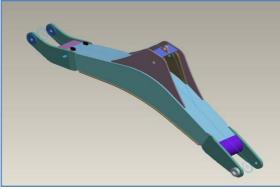


Fig 3.1(a) Boom structure of backhoe loader

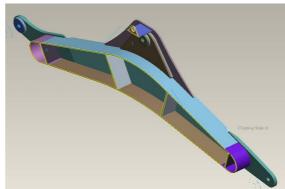


Fig 3.1(b) Cut section view-Boom of backhoe loader

## **3.2 ANALYSIS PROCEDURE**

3.2.1 Analysis Preference: Structural (Static)

#### 3.2.2 Elements used:

| Element       | Remarks  |
|---------------|--|
| SOLID 92      | DOF available: UX, UY, UZ  |
| (10-noded     | SOLID 92 element is giving better accuracy for the model with complex shape.   |
| tetrahedral)  |  |
| SURF 154      | DOF available: UX, UY, UZ  |
| (8-noded)     | Used to define the surface loads like reaction forces of pin                   |
| MASS 21       | DOF available: UX, UY, UZ, Rot X, Rot Y, Rot Z                                 |
| (1-mass node) | Used for introducing additional rotation DOF to solid elements specifically at |
|               | the holding pivots   |
| LINK 8        | DOF available: UX, UY, UZ  |
| (2-noded)     | Used for defining the hydraulic cylinder as rigid link                         |

 Table 3.1 Elements Used for Analysis



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# 3.2.3 Real Constant:

| Element  | Real Constant  |  |  |  |  |  |
|----------|--|--|--|--|--|--|
| SURF 154 | Unit thickness is given in all the nodes                                   |  |  |  |  |  |
|          | TKI = TKJ = TKK = TKL = 1  |  |  |  |  |  |
| MASS 21  | Unit mass in all the directions:   |  |  |  |  |  |
|          | MASS $X = MASS Y = MASS Z = 1$   |  |  |  |  |  |
| LINK 8   | To have high stiffness, cross sectional area more than the actual value is |  |  |  |  |  |
|          | specified.   |  |  |  |  |  |

Table 3.2 Real Constants used for Analysis

#### **3.2.4 Material Properties:**

Elastic modulus =  $2.1 \times 10^5 \text{ N/mm}^2$ ; Poisson's ratio = 0.3

| Part              | Material         |
|-------------------|------------------|
| BOOM STOPPER(13)  | MS010102         |
| LIFTING HOOK((12) | MS010102         |
| ROD BOOM LOCK(14) | MS012008-Fe410WA |
| OTHER PARTS       | MS010201         |

#### Table 3.3 Material Properties considered for Analysis

#### **3.2.5 FE Model Details**:

- The boom stoppers are suppressed for the analysis as they are not the load carrying members.
- The MASS21 is created at the center pivot of the boom swinger and center pivot of the boom cylinder.
- The constraint Equation are defined between Solid 92 and Mass 21 at the Boom swinger The link element is modeled to simulate the tilt of the cylinder as rigid link and the constraint equations are defined between the LINK8, MASS2 and Solid 92 at the boom cylinder pivot



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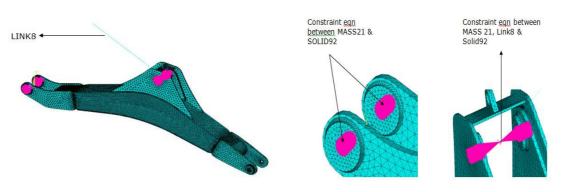


Fig 3.2(a) Figure shows FE Model links

Fig 3.2(b)Figure shows FE Model Constraints

## 3.3 BOUNDARY CONDITION:

- The boom swing pivot side is given hinged condition and all the translational DOF and X & Y rotation DOF are arrested at this hinged support.
- Both end of the link is fixed arresting all DOF

## 3.4 LOADING CONDITION:

#### Load case1:

#### **Crowding condition:**

In crowding condition, the force of 297400 N are applied at the boom arm pivot. These forces are resolved into two components ( $F_x$  and  $F_y$ ) and applied as surface load (pressure) along X and Y directions.

|       |                   | Area(A)<br>mm <sup>2</sup> | Force, N                  |                     | Pressure, N/mm <sup>2</sup> |                 |
|-------|-------------------|----------------------------|---------------------------|---------------------|-----------------------------|-----------------|
| S.no  | Load per side     |                            | $F_x\!\!=\!\!F\cos\theta$ | $F_{y}=F\sin\theta$ | $P_x = F_x / A$             | $P_y = F_y / A$ |
| 6.2.1 | 297400 N/2<br>12° | 1374.4                     | 145450.4589               | 30916.468           | 105.82                      | 22.49           |

Table 3.4 Shows loads applied during Crowding Condition



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### Load case2: Digging condition:

In digging condition, the force of 256600 N is applied at the boom arm pivot. These force are resolved into two components ( $F_x$  and  $F_y$ ) and applied as surface load (pressure) along X and Y directions.

|       |               | Area(A)<br>mm <sup>2</sup> | Force, N              |                     | Pressure, N/mm <sup>2</sup> |               |
|-------|---------------|----------------------------|-----------------------|---------------------|-----------------------------|---------------|
| S.no  | Load per side |                            | $F_x = F \cos \theta$ | $F_y = Fsin \theta$ | $P_x = F_x / A$             | $P_y = F_y/A$ |
| 6.2.2 | 256600N /2    | 1374.4                     | 127051.393            | 17855.908           | 92.44                       | 12.99         |

Table 3.5 Shows loads applied during Digging Condition

## **IV. RESULTS AND DISCUSSIONS**

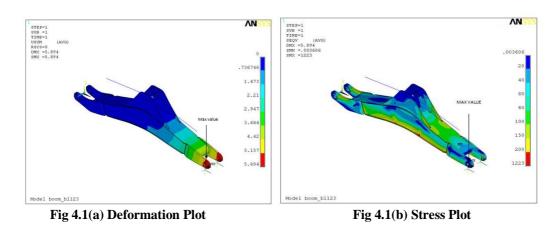
# Load case 1:

**Deformation plot:** 

The deformation plot for this load case is given in fig.4.1(a)The Maximum deflection is 5.894 on the End Lug Plate

# Stress plot:

The maximum value of von mises stress is  $1223 \text{ N/mm}^2$  at the weld between Bottom Plate and arm end lug plate .The high stress is due to singularity error shown in fig 4.1(b)





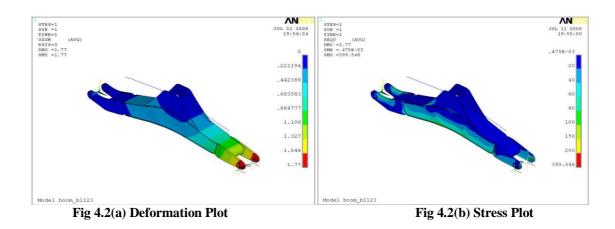
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Load case2: Deformation Plot: The Maximum deflection is 1.77 on the Arm End Lug Plate.

#### **Stress Plot:**

The maximum value of von mises stress is 399.548 N/mm<sup>2</sup> at the weld between Bottom Plate and arm end lug plate (lhs). The high stress is due to singularity error.



#### V. CONCLUSION

The Deformation and Stress plot for the Backhoe Boom are obtained from the above analysis. The stresses are less than the fatigue strength of the material.

The design of Backhoe Boom assembly is ok.

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