

# Strip Thickness Control of Cold Rolling Mill

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**ABSTRACT:** It's possible for different kinds of automatic gauge control (AGC) systems working simultaneously to impact and disturb each other while adjusting their moving directions. In order to implement a decoupling control, we modified the parameters and structure of the AGC system in a hot rolling mill. In rolling mill, the accuracy and quality of the strip exit thickness are very important factors. To realize high accuracy in the strip exit thickness, the Automatic Gauge Control (AGC) system is used. Because of roll eccentricity in backup rolls, the exit thickness deviates periodically. In this paper, we design PI controller in outer loop for the strip exit thickness while PD controller is used in inner loop for the work roll actuator position. Also, in order to reduce the periodic thickness deviation, we propose roll eccentricity compensation by using Fuzzy Neural Network with online tuning. Simulink model for the overall system has been implemented using MAT-LAB/SIMULINK software. The simulation results show the effectiveness of the proposed control.

**KEYWORDS:** Cold Rolling Mill; Thickness Control; Roll Eccentricity; Eccentricity Compensation

## 1. INTRODUCTION

Rolling strip is widely used for automobile manufacturing, food packaging, household electric appliances, machinery, light industry, instruments, communications, military affairs and other fields [1]. The design of a controller in the cold rolling system that can improve the behavior and response of the plant to specific performance constraints can be a tedious and challenging problem in many control applications [2]. In order to meet increasing demand for the high precision of strip thickness, various types of Automatic Gauge Control (AGC) methods have been developed for hot or cold mill processes. The British Iron and Steel Research Association (BISRA) AGC method based on the gauge meter principle and the feed forward AGC method using the delivery time of the strip have been widely utilized in steel rolling mills [3].

Strip products thickness precision is an important quality parameter. But the export thickness appears as the periodical fluctuation in the practical production because of the roll eccentricity thermal expansion of rolls and the fluctuation of the entrance thickness and material stiffness. The mill can be composed of either a single stand or a number of stands where each stand is made up of two back-up rolls and two work rolls. A common problem is the back-up and work rolls are not perfectly circular in shape. In other words, the rolls are eccentric. The roll eccentricity effect will, under normal constant operating forces, result in steel strip with undesirable thickness deviation. In this paper, PI and PD controller has been used to control the output thickness and hydraulic servo system respectively. Also we propose roll eccentricity compensation by using Fuzzy Neural Network. The paper is organized as follows: in Section 2, a brief description of the cold rolling process is presented. In Section 3, a mathematical model has been driven for single-stand cold rolling mill. In Section 4, architecture and learning algorithm of Fuzzy Neural Network have been presented. In Section 5, thickness control with roll eccentricity compensation has been proposed. In Section 6, simulation results have been presented. Finally, section 7 presents the conclusions.

## II. COLD ROLLING PROCESS OVERVIEW

The tandem cold rolling of metal strip is one process in a sequence of processes performed to convert raw materials into a finished product [6]. It is a deformation process in which the thickness of the strip is reduced by compressive

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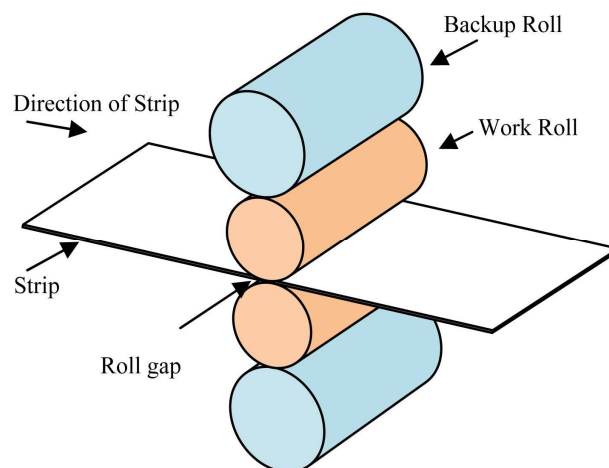
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forces exerted by two opposing rolls (two or four-high arrangement of rolled products). The roll rotates as illustrated in **Figure 1** to pull and simultaneously squeeze the strip between them [7].

The strip is passed through four pairs of independently driven work rolls, with each work roll supported by a backup roll of larger diameter. As the strip passes through the individual pairs of work rolls, the thickness is successively reduced. The reduction in thickness is caused by very high compression stress in a small region (denoted as the roll gap, or the roll bite) between the work rolls. In this region the metal is plastically deformed, and there is slipping between the strip and the work roll surface. The necessary compression force is applied by hydraulic rams, or in many older mills by a screw arrangement driven by an electric motor [6].



**Figure 1. The rolling process (flat rolling)**

### III. MATHEMATICAL MODEL OF COLD ROLLING PROCESS

#### A. FORCE EQUATION

Define the theory for prediction of specific roll force is central to the development of a model for tandem cold rolling. Referring to **Figure 2**, which approximately represents the strip in the roll bite area, the incoming strip is of thickness  $h_{in}$  at its centerline and is moving toward the roll bite with speed  $v_{in}$ . The strip exits the roll bite with thickness  $h_{out}$  at its centerline and with speed  $v_{out}$  [6,7]. In flat rolling, the strip is squeezed between two rolls so that its thickness is reduced by an amount called the draft [7]:

$$d = h_{in} - h_{out} \quad (1)$$

where  $d$  = draft, mm.

The rolling strip contact length can be approximated by [8]:

$$L = \sqrt{R(h_{in} - h_{out})} \quad (2)$$

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The true strain experienced by the strip in rolling is based on before and after stock thickness. In equation form:

$$\epsilon = \ln \frac{h_{in}}{h_{out}} \quad (3)$$

The true strain can be used to determine the average flow stress  $Y_{avg}$  applied to the strip material in flat roll-ing:

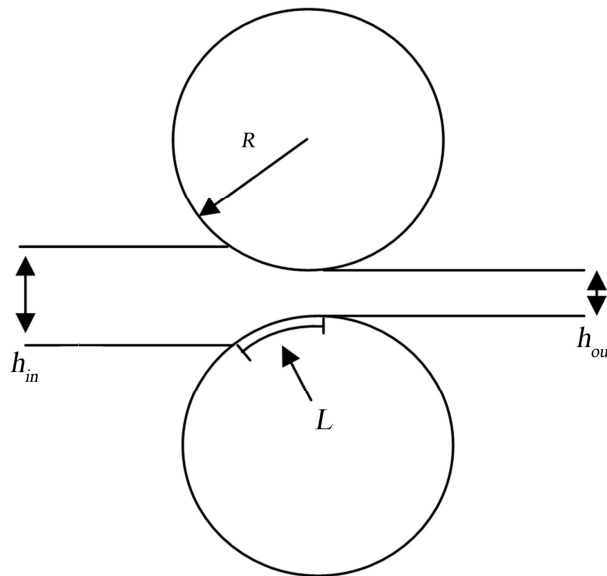


Figure 2. Roll bite area.

$$Y_{avg} = K \epsilon^n \quad (4)$$

where  $K$  = the strength coefficient, MPa; and  $n$  is the strain hardening exponent.

The force  $F$  required to maintain separation between the two rolls can be calculated based on the average flow stress experienced by the strip material in the roll gap [7,8]. That is,

$$F = Y_{avg} wL \quad (5)$$

where  $w$  = width of the strip,  $R$  is radius of work roll.

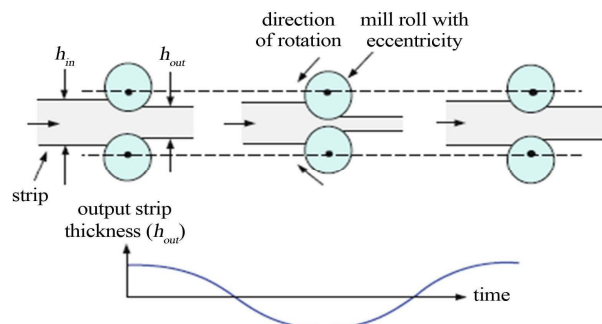


Figure 3. Effects of roll eccentricity on output strip thickness

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### B. OUTPUT THICKNESS EQUATION

In the cold rolling process and the precision is strip thickness of cold rolled strips of key quality products. Conventional Automatic roll gap Control (where Gauge, AGC) system used for Automatic correction strip thick-ness accuracy [9]. One of the conventional control strat-egy of strip thickness is using of BISRA measurements to infer strip thickness. This relationship (more often referred to as “gaugemeter” or “BISRA gaugemeter”) has been used to estimate the thickness of the strip exiting the roll bite without requiring a direct measurement. Re-liable direct measurement of strip thickness at the exit of the roll bite requires expensive and complex equipment [6]. The relationship between the work roll gap( $S$ ), the exit strip thickness  $h_{out}$ , and the roll force( $F$ ) generated at the roll stand is expressed as [3,10]:

$$h_{out} = S + \frac{F}{M} \quad (5)$$

where  $M$  is mill modulus

The BISRA relationship is used to develop a thickness feedback signal for closed-loop control. To control the output thickness, the motion of hydraulic cylinder con-trolling the roll gap position is such that produces the desired output thickness [6]. Roll eccentricities are caused by axial deviations between the roll barrel and the roll necks due to irregularities in the mill rolls and/or roll bearings [11]. These irregularities cause cyclic deviations in the strip thickness at the output of a mill stand. **Figure 3** depicts the effects of eccentricity on the output strip thickness [6].

When the entry strip is passed through the roll stand with the velocity  $v_{in}$ , the disturbance  $\Delta H$  is expressed as:

$$\Delta H = A_d \sin \frac{2\pi v_{in} t}{L_d} \quad (6)$$

where  $A_d$  and  $L_d$  are the magnitude and period of thickness deviation respectively [3]. Roll eccentricity is not part of the controller but must be considered to be consistent with data reported from operating mills which

usually includes its effects. The eccentricity components remaining in the mill exit thickness after compensation. In the model, roll eccentricity modifies Equation (5) as [12]:

$$h_{out} = S + \frac{F}{M} + e \quad (7)$$

where  $e$  is the roll eccentricity.

### IV. DESIGN OF THICKNESS CONTROL WITH ROLL ECCENTRICITY COMPENSATION

The block diagram of exit thickness control with roll eccentricity compensation is shown in **Figure 5**. As an inner loop of Hydraulic AGC System, the difference value between desired position roll gap and the real posi-tion measured by displacement sensor of hydraulic cy-linder is input to APC controller. Automatic position control (APC) can affect the exit thickness by controlling the position of hydraulic cylinder [1]. The main compo-nents of hydraulic screw down servo system include con-troller, servo amplifier, servo valve, hydraulic cylinder, roller system and body of rolling mill, and some sensors [19]. In the outer loop, the difference between desired thickness and output thickness is fed to AGC to give the desired position roll gap. Fuzzy Neural Network system have been used with online training to compensation the effect of roll eccentricity. The first input of the Fuzzy Neural Network system is output thickness and the second input is change of output thickness. The output of the Fuzzy Neural Network system (c) added to the de-

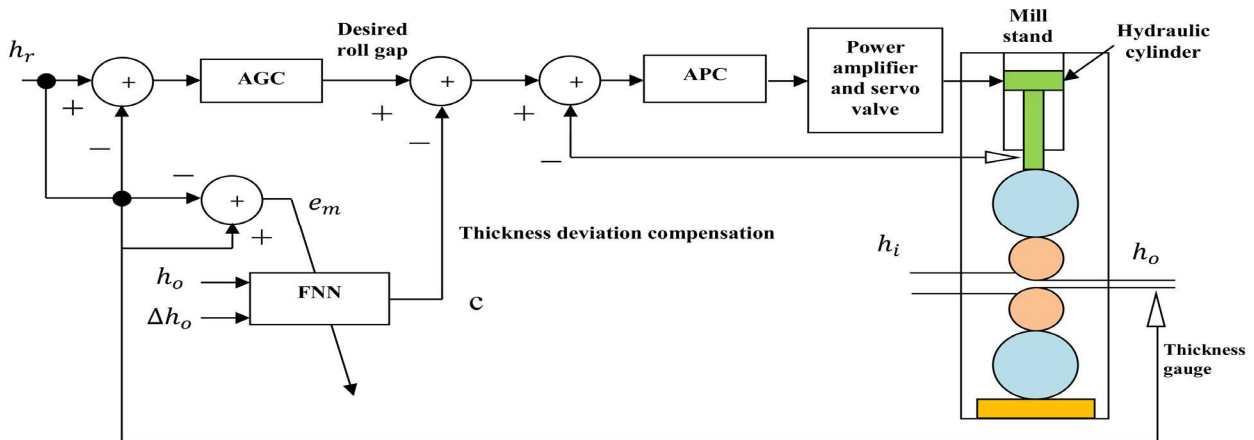
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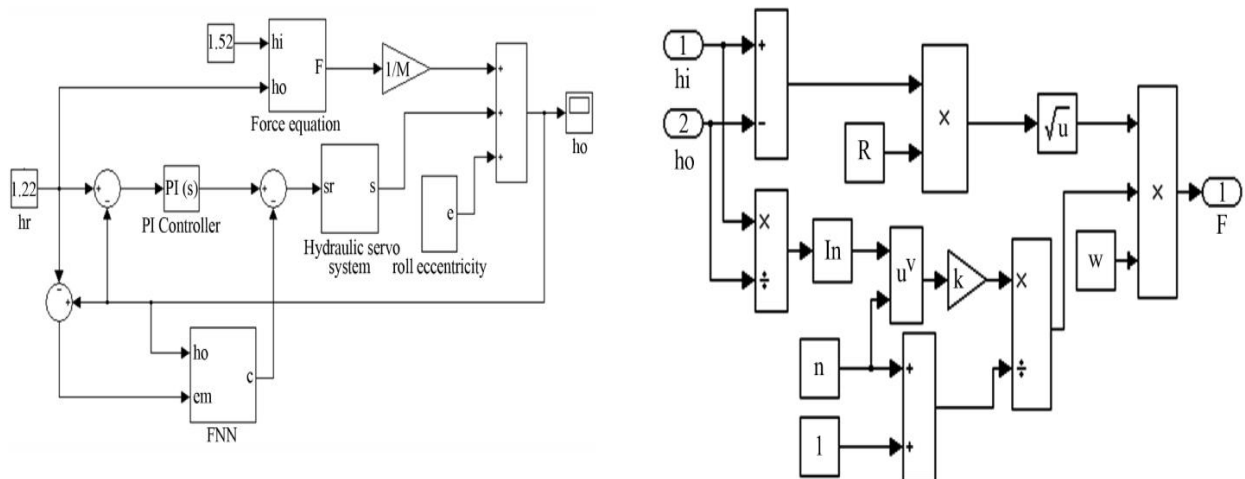
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sired position to regulate the roll gap and then reducing the periodic thickness deviation.  $e_m$  is the error between desired output thickness and output thickness of the stand that used as trajectory in adaptive mechanism. SIMU-LINK model of thickness control have been implemented using MATLAB/SIMULINK software as shown in **Figure 6**. PI controller is used as AGC and PD controller is



**Figure 5. Block diagram of exit thickness control.**



**Figure 6. Simulink model of thickness control.**

used as APC.

The simulink model of force equation is shown in **Figure 7**. Also the simulink model of hydraulic servo system is shown in fig.

## V. SIMULATION RESULTS

A program written in Matlab code is used to simulate FNN using Matlab S-function programming. In the primes part, the number of membership functions for each input are five. So, the number of weights in the consequence part is also five. The mill and strip proper-ties is shown in **Table 1**. Without roll eccentricity effect, **Figure** shows the exit

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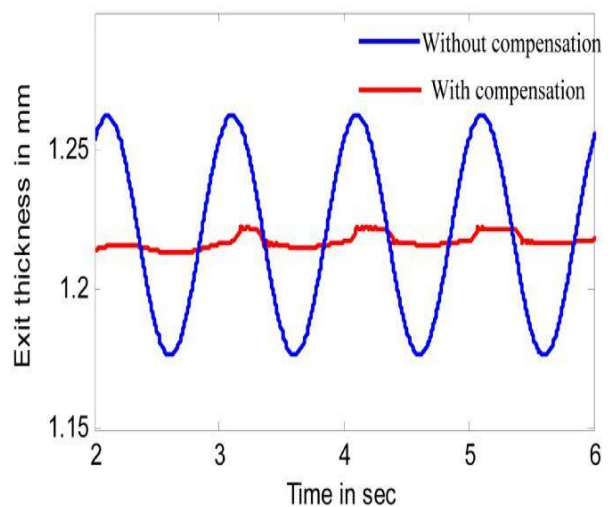
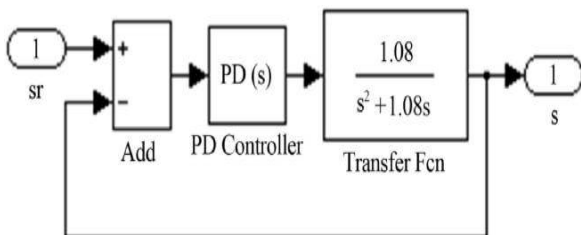
thickness when the desired thickness is 1.22 mm. When roll eccentricity is taken into account, the exit thickness is shown in **Figure 11**. As shown in this figure, the disturbance ( $\Delta H$ ) which has

Amplitude  $A_d$  appear periodically in the exit thickness and this is drawback that effect on the accuracy and qual-ity of the strip exit thickness. The compensation signal (c) which is produced by FNN added to the desired position roll gap to reduce the periodic deviation in the exit thickness. This is shown clearly in **Simulink model of force equation**.

**Table 1. The mill and strip properties.**

Parameter	Dimension
Work roll radius	250 mm
Mill modulus	3921 kN/mm
Strip width	600 mm
Entry Thickness	1.52 mm
Exit thickness	1.22 mm
strength coefficient	240 MPa
strain hardening exponent	0.15
$A_d$	0.05 mm
$v_{in}$	2 m/s
$L_d$	2 m

shows the exit thickness after cancellation the effect of roll eccentricity. The exit thickness with and without compensation is shown in **Figure 12**. From simulation



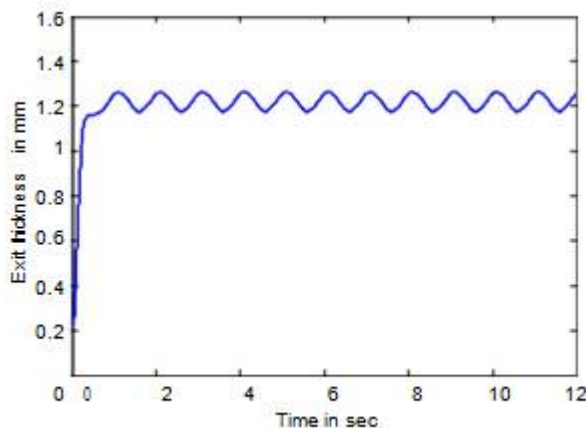
**Exit thickness with and without compensation.**

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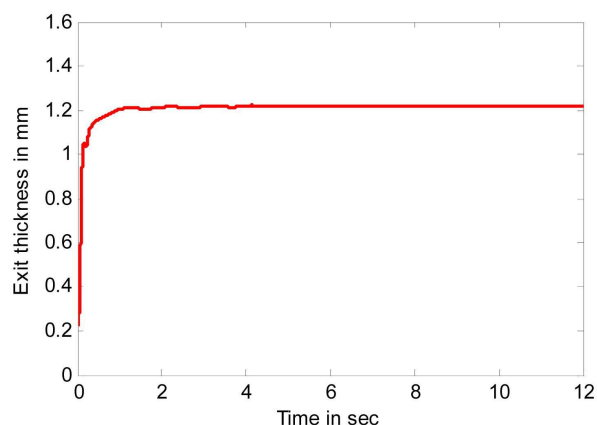
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**Exit thickness with roll eccentricity effect.**



**. Exit thickness after compensation the effect of roll eccentricity.**

results, It is found that FNN is robust in that it eliminate the periodic thickness deviation considerably.

## VI. CONCLUSION

In this paper, the mathematical model of single-stand cold rolling mill is developed and PI controller has been used to control exit thickness of the strip. We propose FNN in order to reduce the effect of roll eccentricity. The error between the reference exit thickness and output thickness of stand is used as trajectory to adapt the primes part and the consequence part of the FNN so that the error goes toward zero. The output of FNN is added to the desired position roll gap to reduce periodic deviation in the output thickness. As we have shown in the simulation results, the performance of proposed method is good.

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